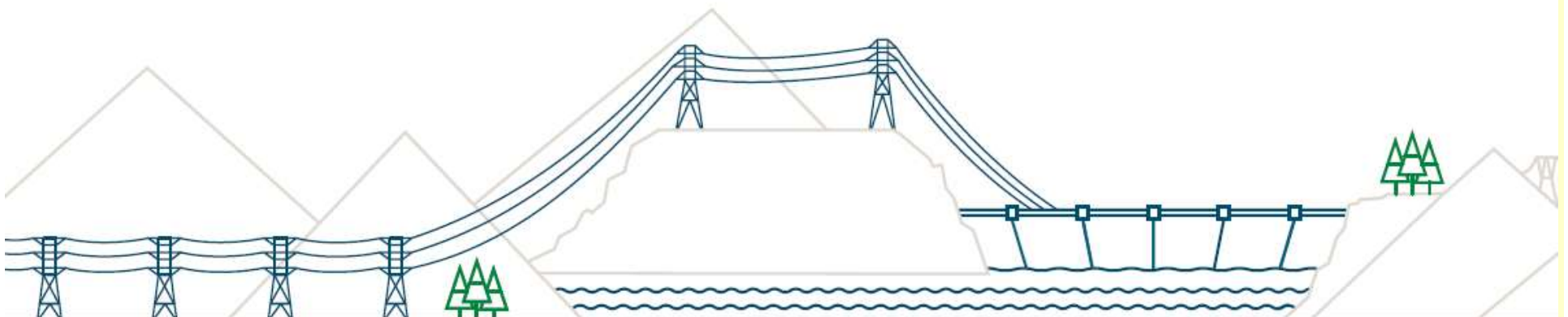


# Severe Overvoltage During Single-Phase Open Period

Mukesh Nagpal, Ph.D., P. Eng.  
BC Hydro



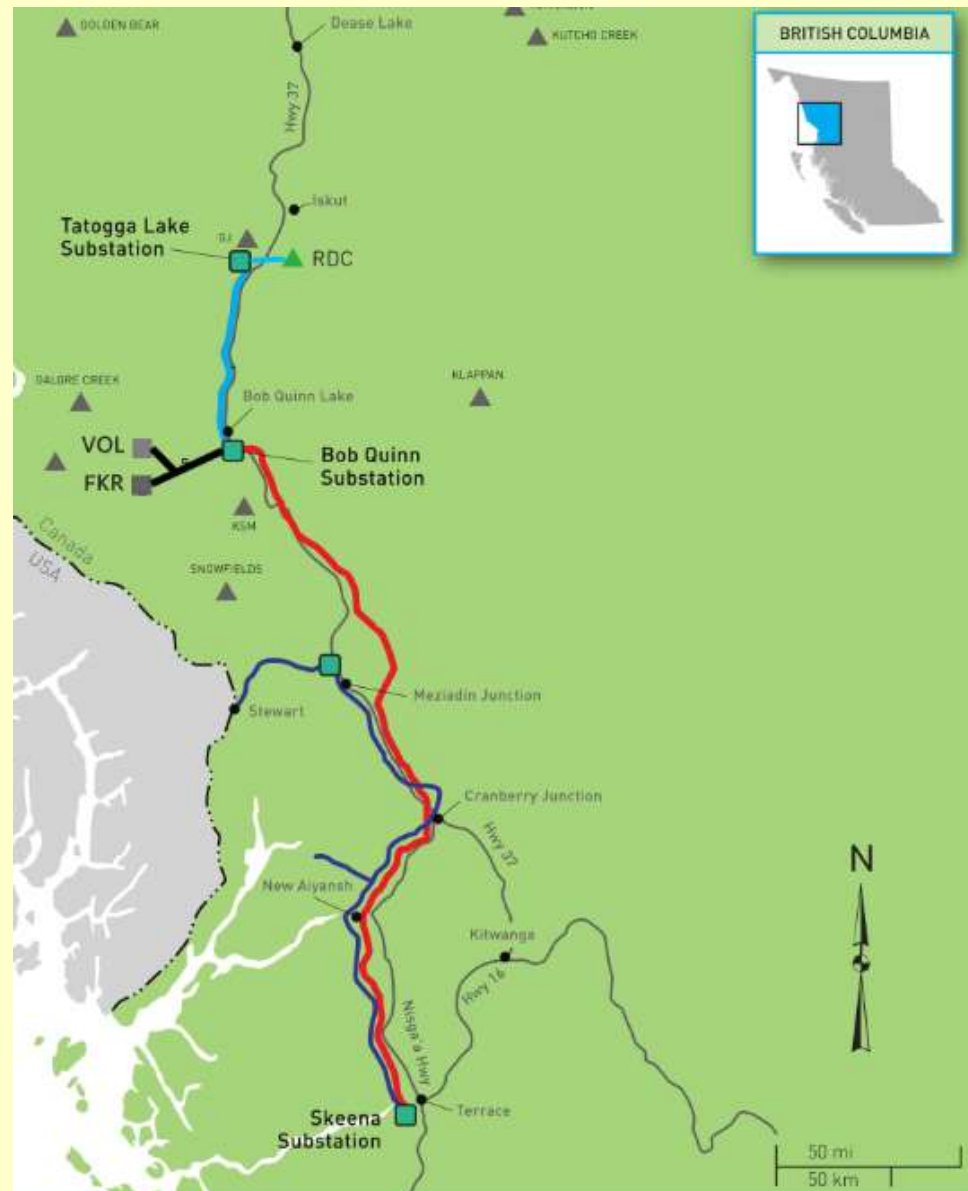
# Outline

- The Northwest Transmission System (NTL)
- What system events happened on January 7<sup>th</sup>?
  - Single-Phase Auto-reclose - Background
- What did protection do during those events?
  - Overexcited Transformer - Background
- System analysis
- Solutions

# NTL

## Three 287 kV lines

BC Hydro System



# 2L102

## 287 kV – 340 km



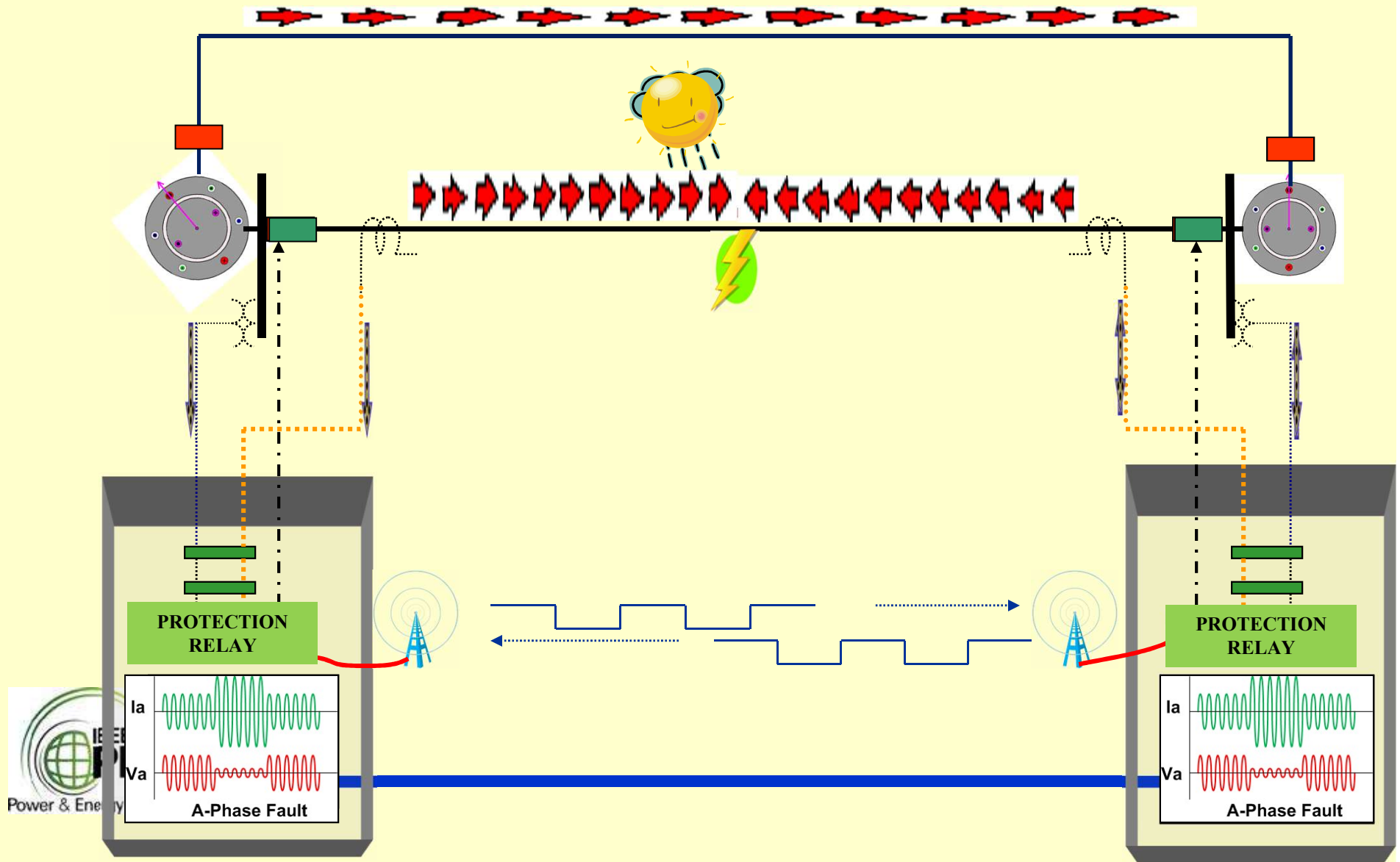
BC Hydro System

### Connects Skeena (SKA) to Bob Quinn (BQN)

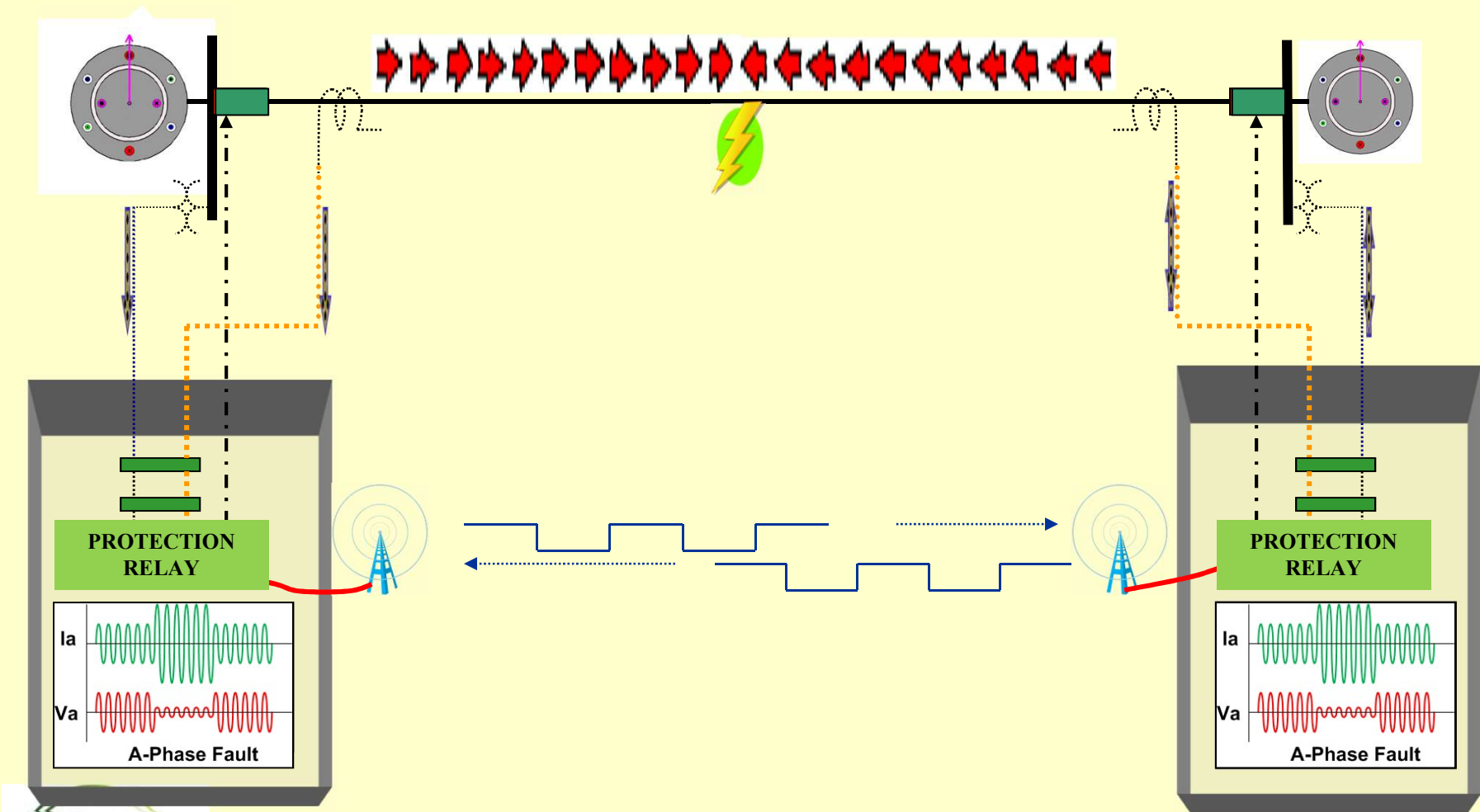
- Line current differential protection
- **Single-pole tripping**
- Optical ground wire
- 2<sup>nd</sup> longest line in BC Hydro
- 35% series capacitor compensation at BQN end
- 84% shunt compensated

# **Three-phase versus Single-phase Trip and Reclose**

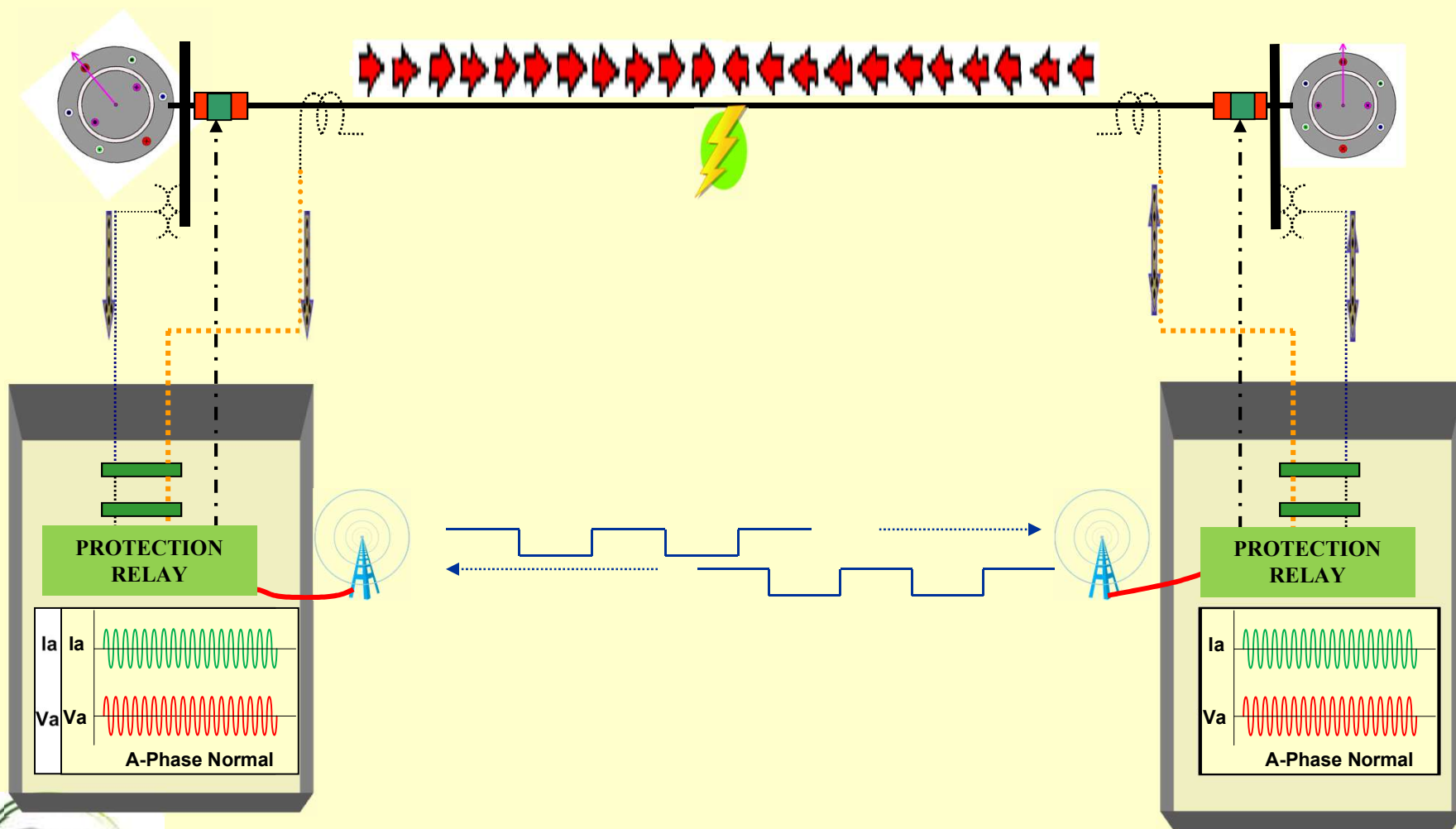
# Three-Phase Auto-Reclosing



# Three-Phase Auto-Reclosing

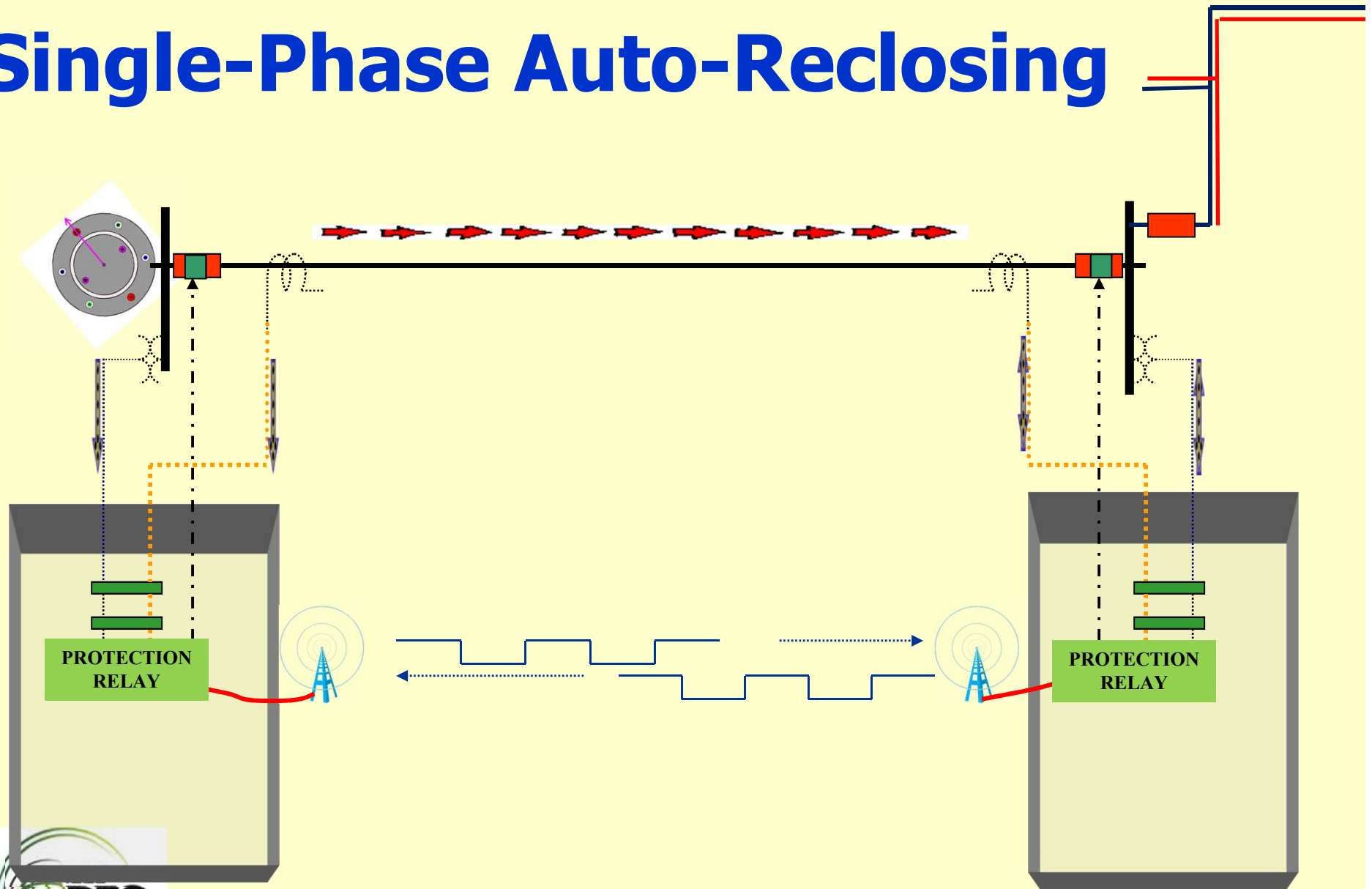


# Single-Phase Auto-Reclosing





# Single-Phase Auto-Reclosing



# Events of January 7th

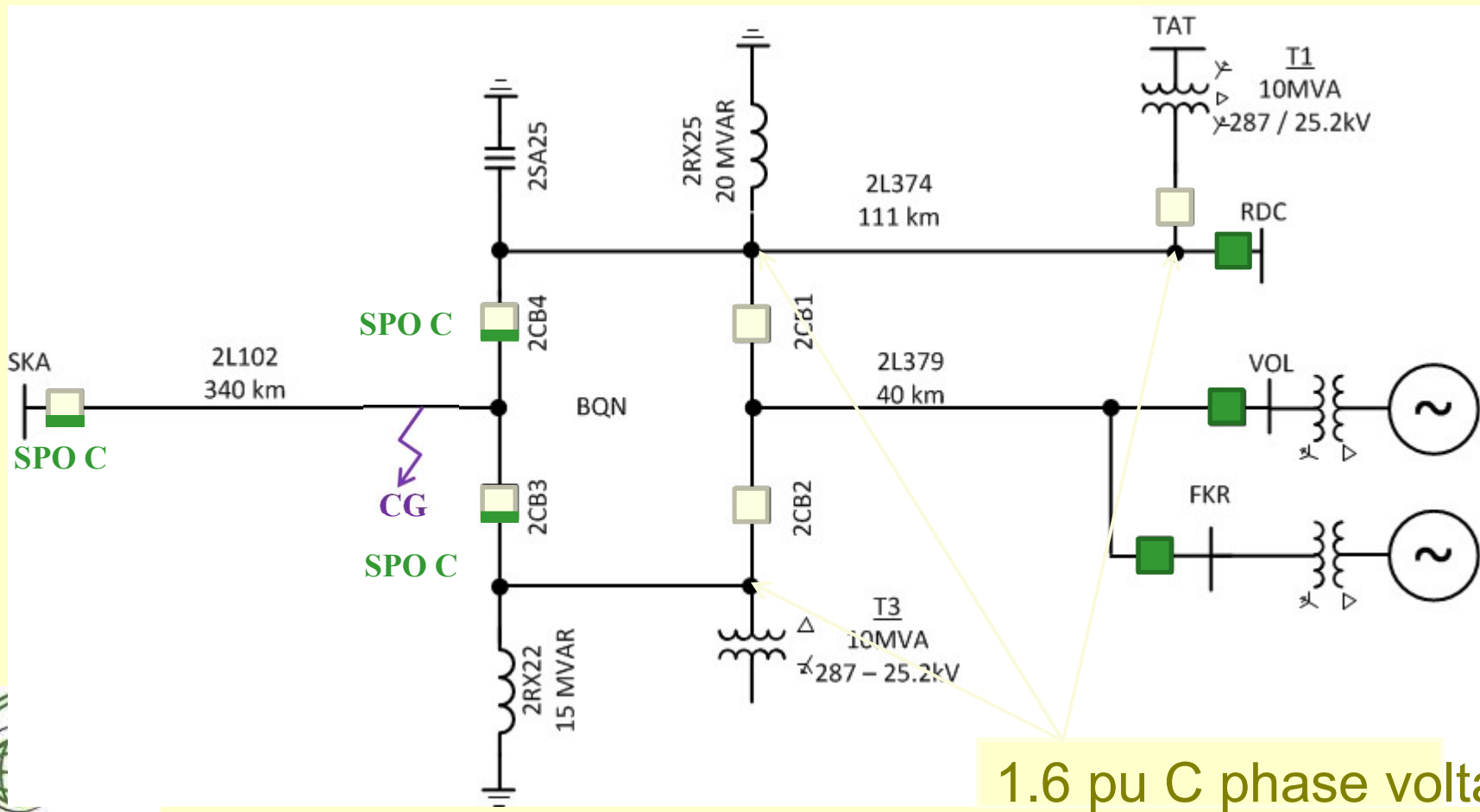


## Event 5 6:21 AM



# Morning of Faults

## Event 5 6:21 AM



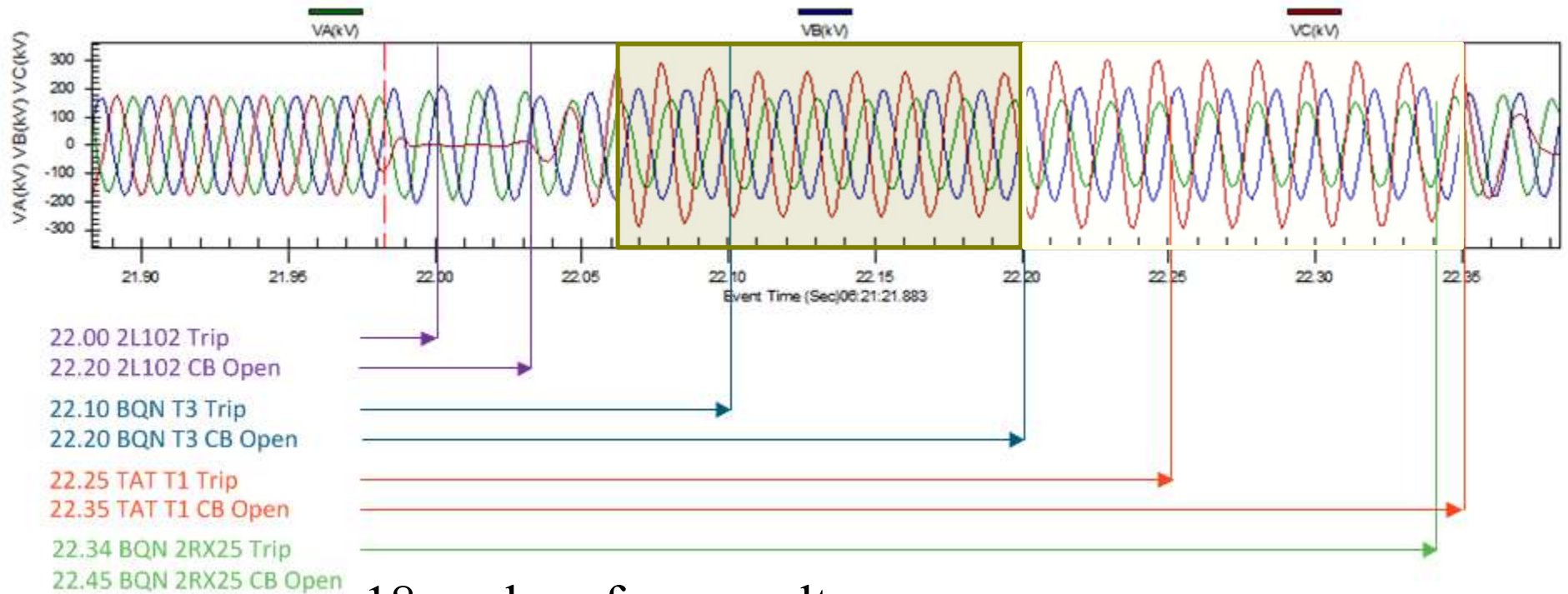
## Event 5 6:21 AM



# Composite Protection Operations

1.6 pu

1.7 pu

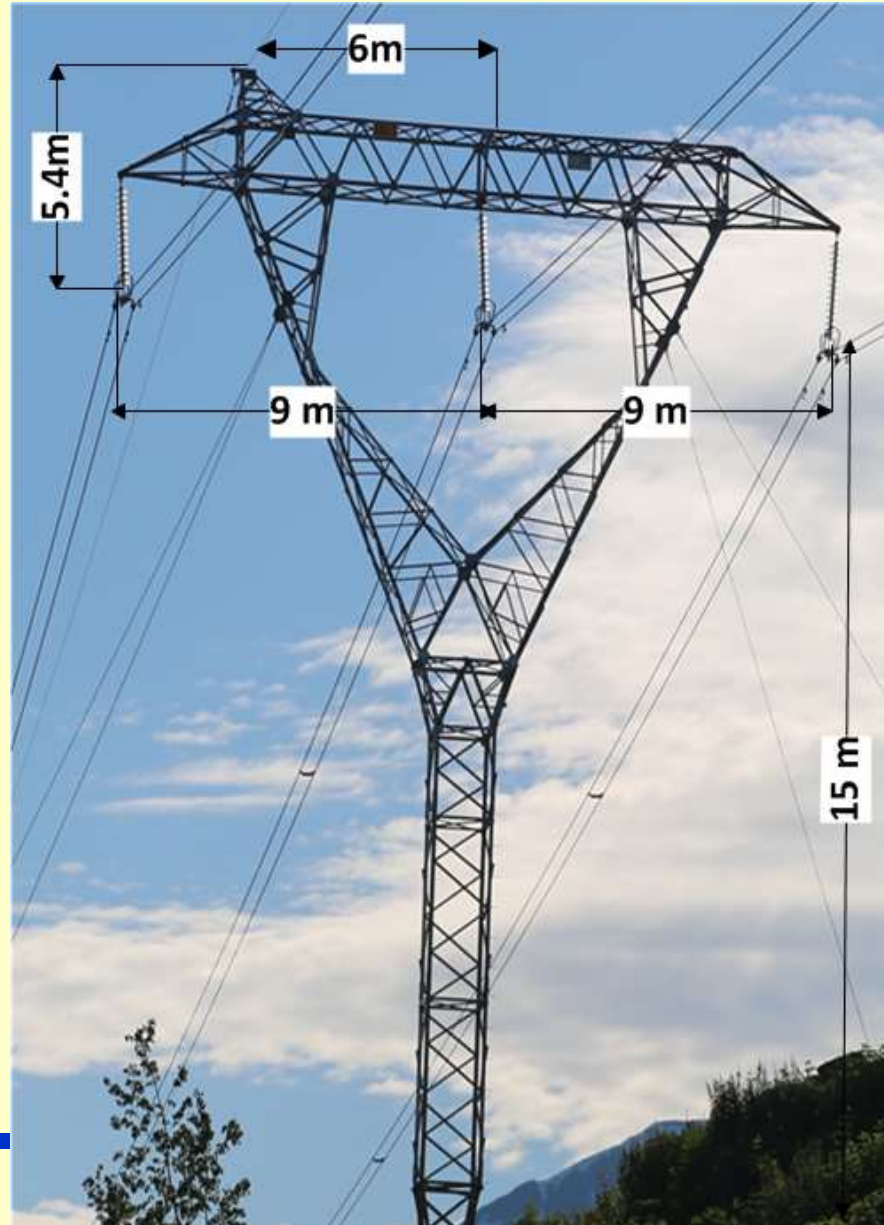


18 cycles of over-voltage

Voltage increased from 1.6 to 1.7 pu when BQN T3 and 2RX 22 tripped off

# Tower Configuration

5.4 m vertical  
separation between  
conductor and  
3.0 m horizontal  
separation between  
conductor and  
OPGW





# OPGW at point of fault

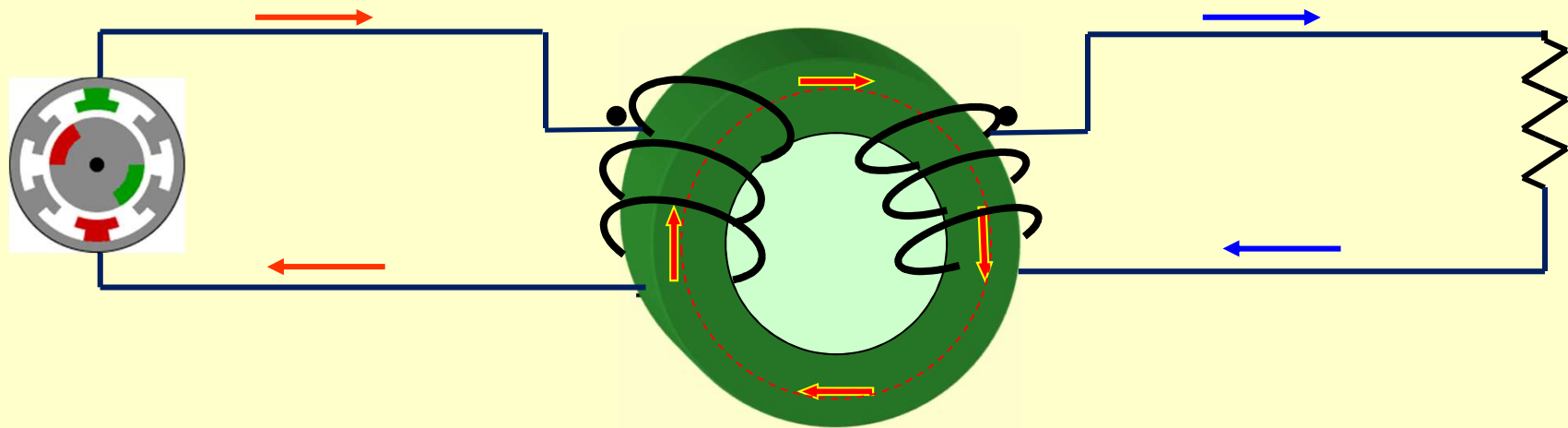




# Transformer Protection Operations

There were two transformer protection operations for no internal faults. While one of them was fortuitous, yet they were baffling because they were designed not to operate on overvoltage as per our standard practice. So they were thoroughly investigated to assess if there was any reliability risk to BC Hydro.

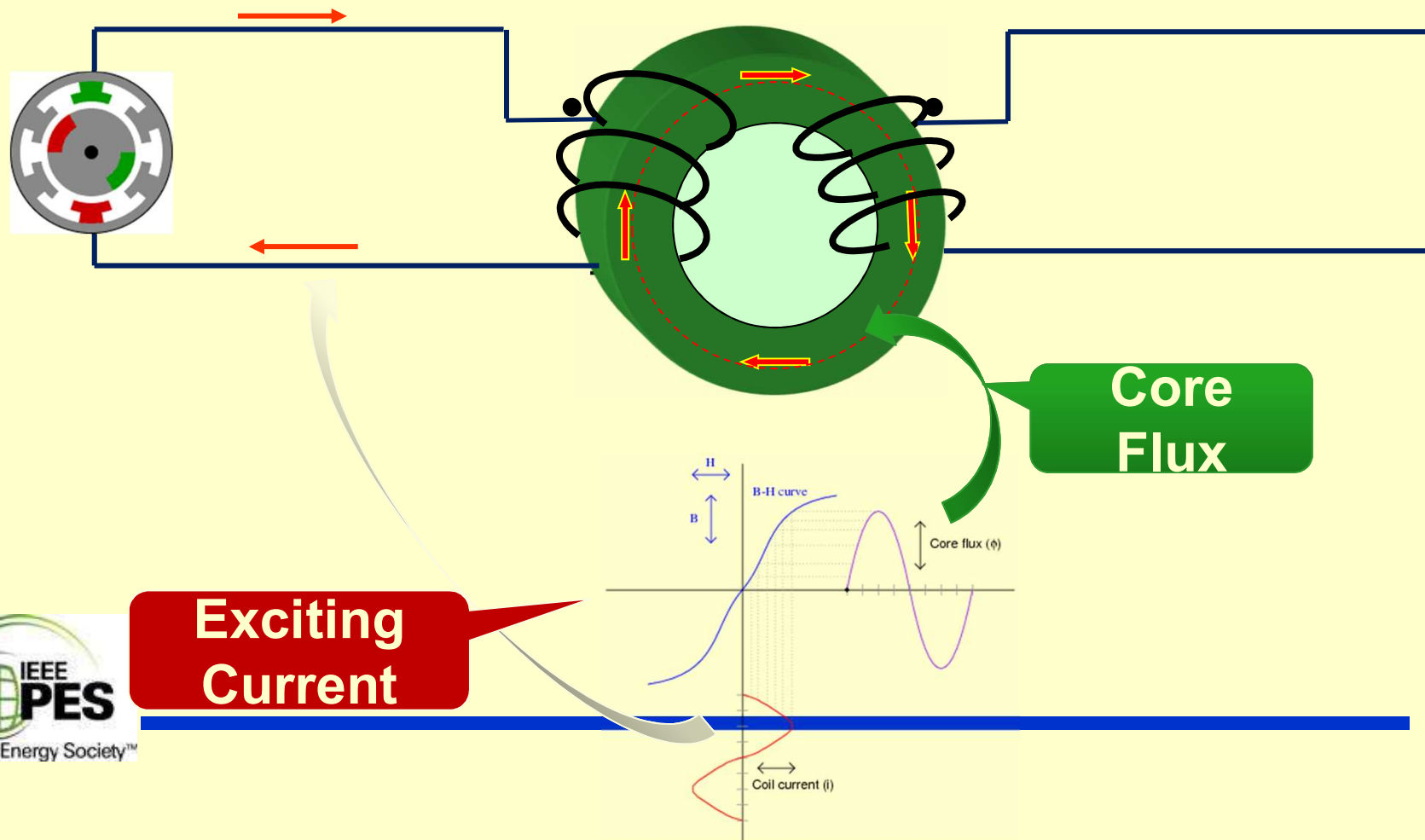
# Transformer Differential Protection



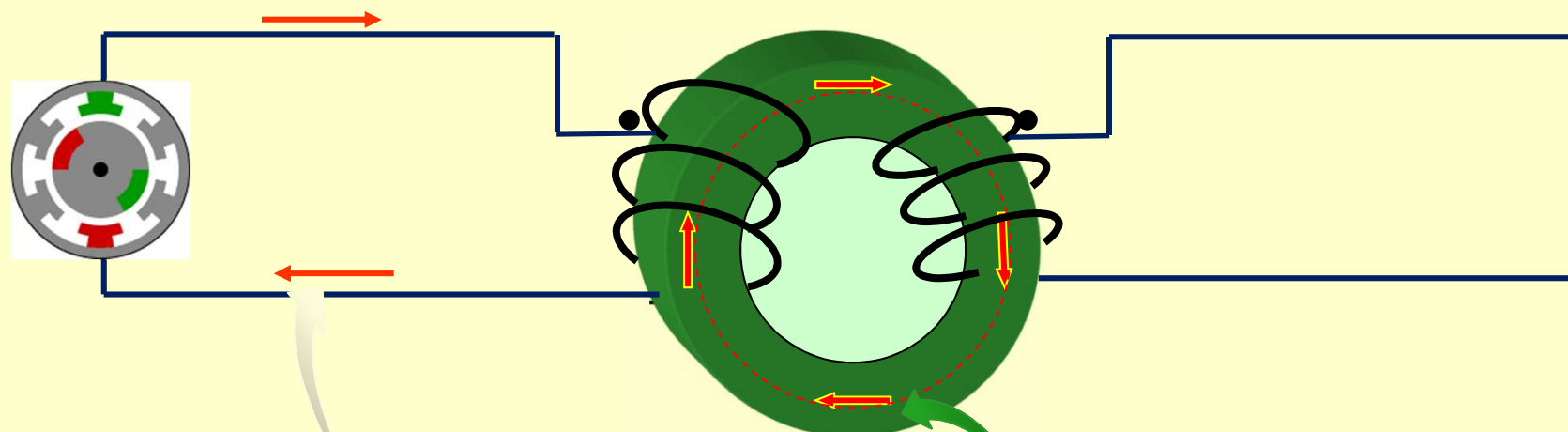
## Healthy Transformer:

Primary ampere turns (1-3% of rating) are slightly higher to establish the magnetizing flux.

# Transformer at No Load

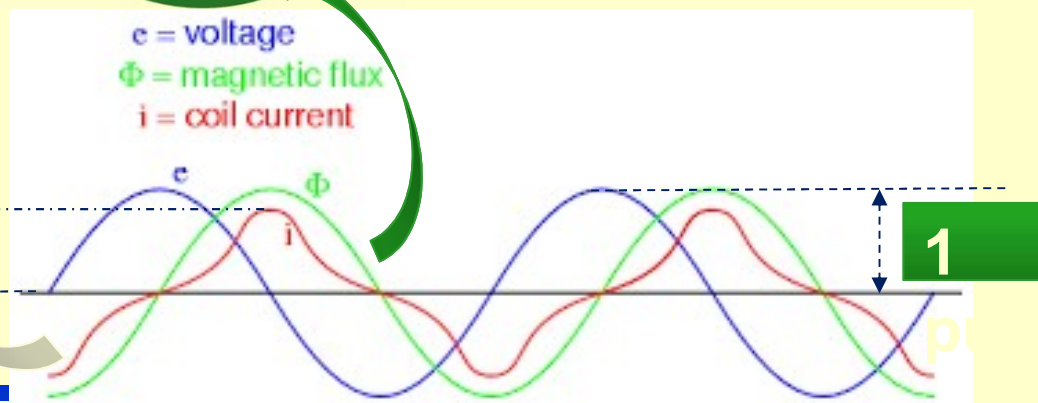


# Transformer at No Load

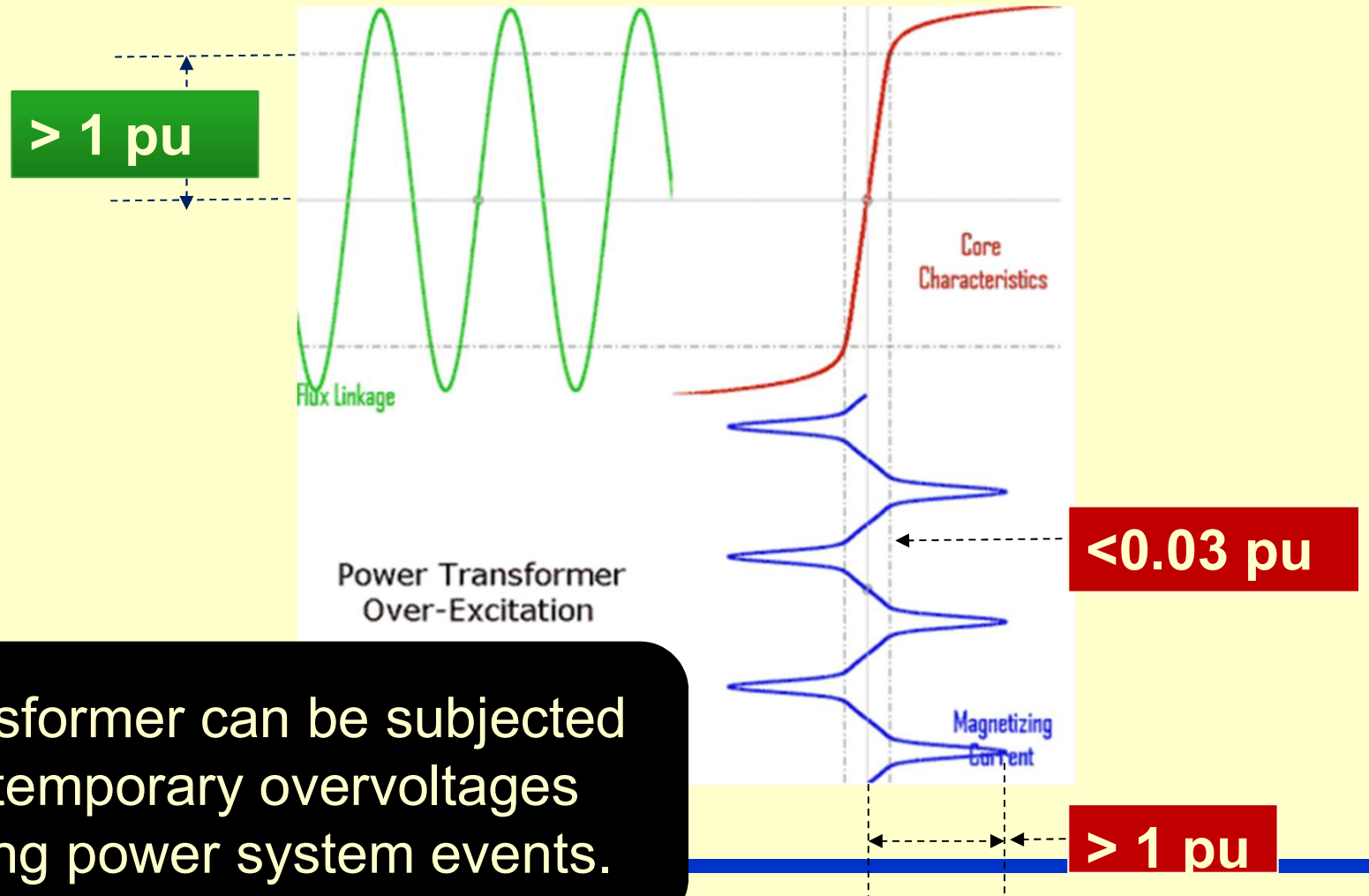


$e$  = voltage  
 $\Phi$  = magnetic flux  
 $i$  = coil current

**<0.03 pu**

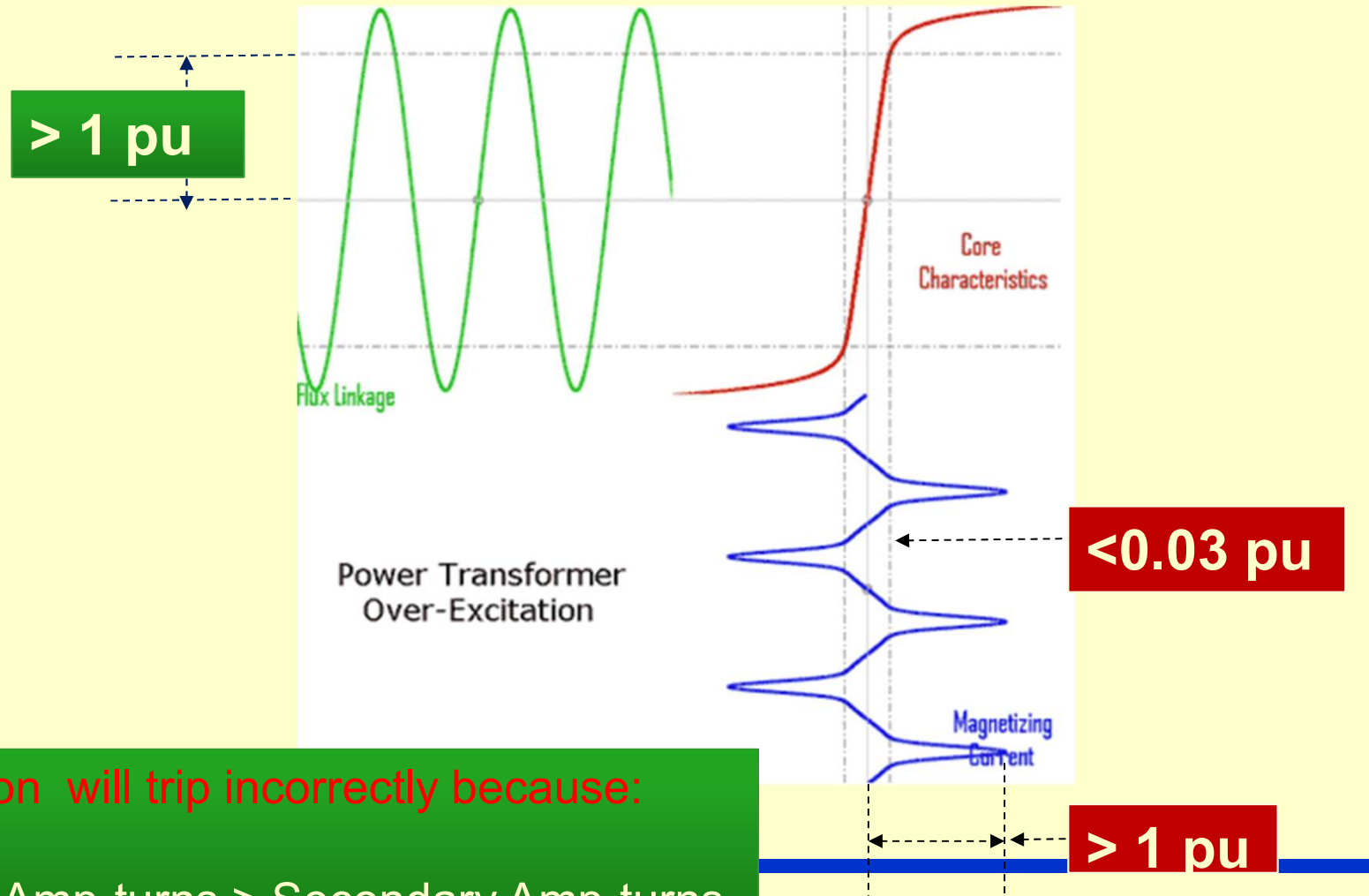


# Transformer Overexcitation Current



Transformer can be subjected to temporary overvoltages during power system events.

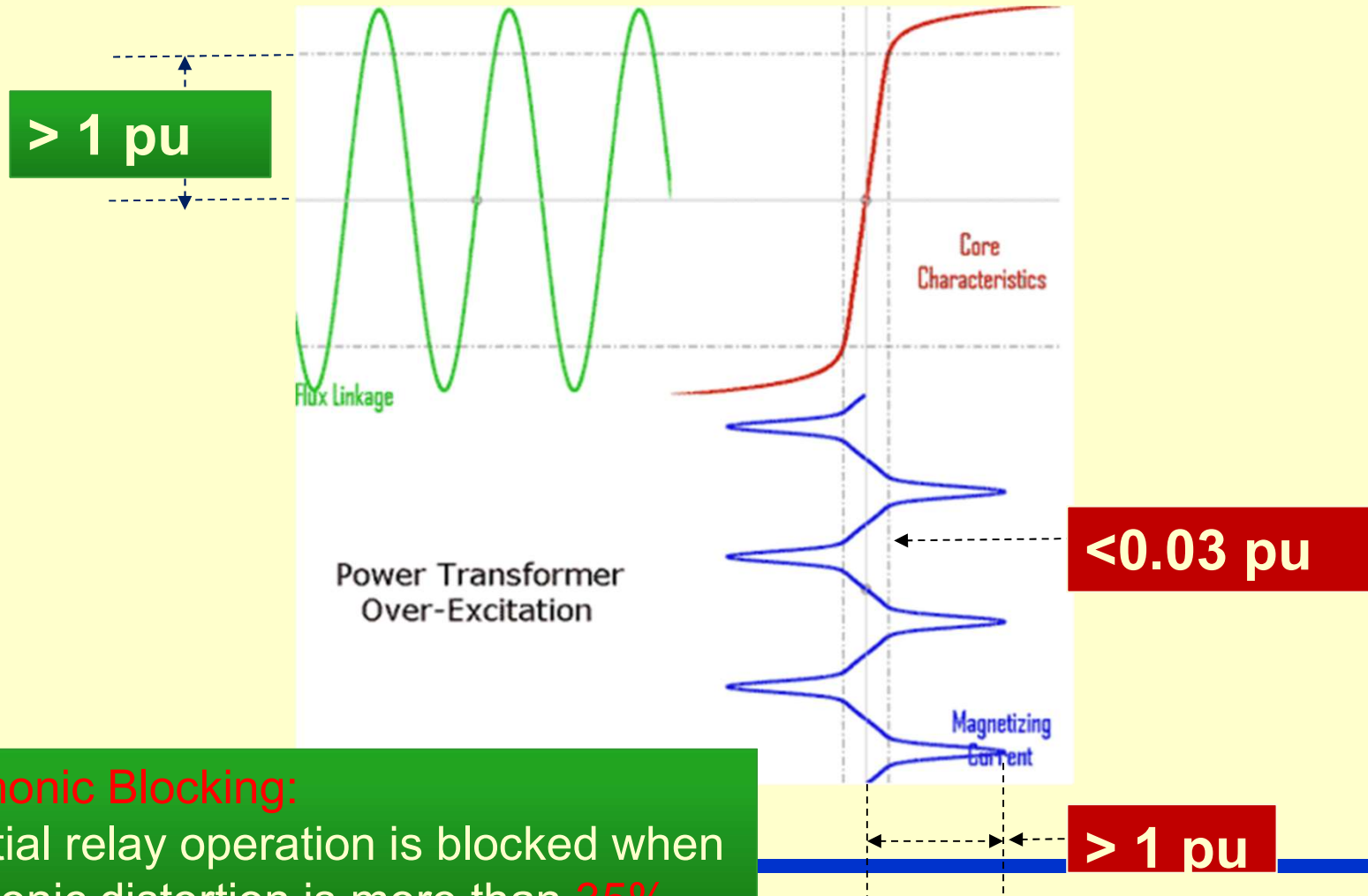
# Transformer Differential Protection



Protection will trip incorrectly because:

Primary Amp-turns > Secondary Amp-turns

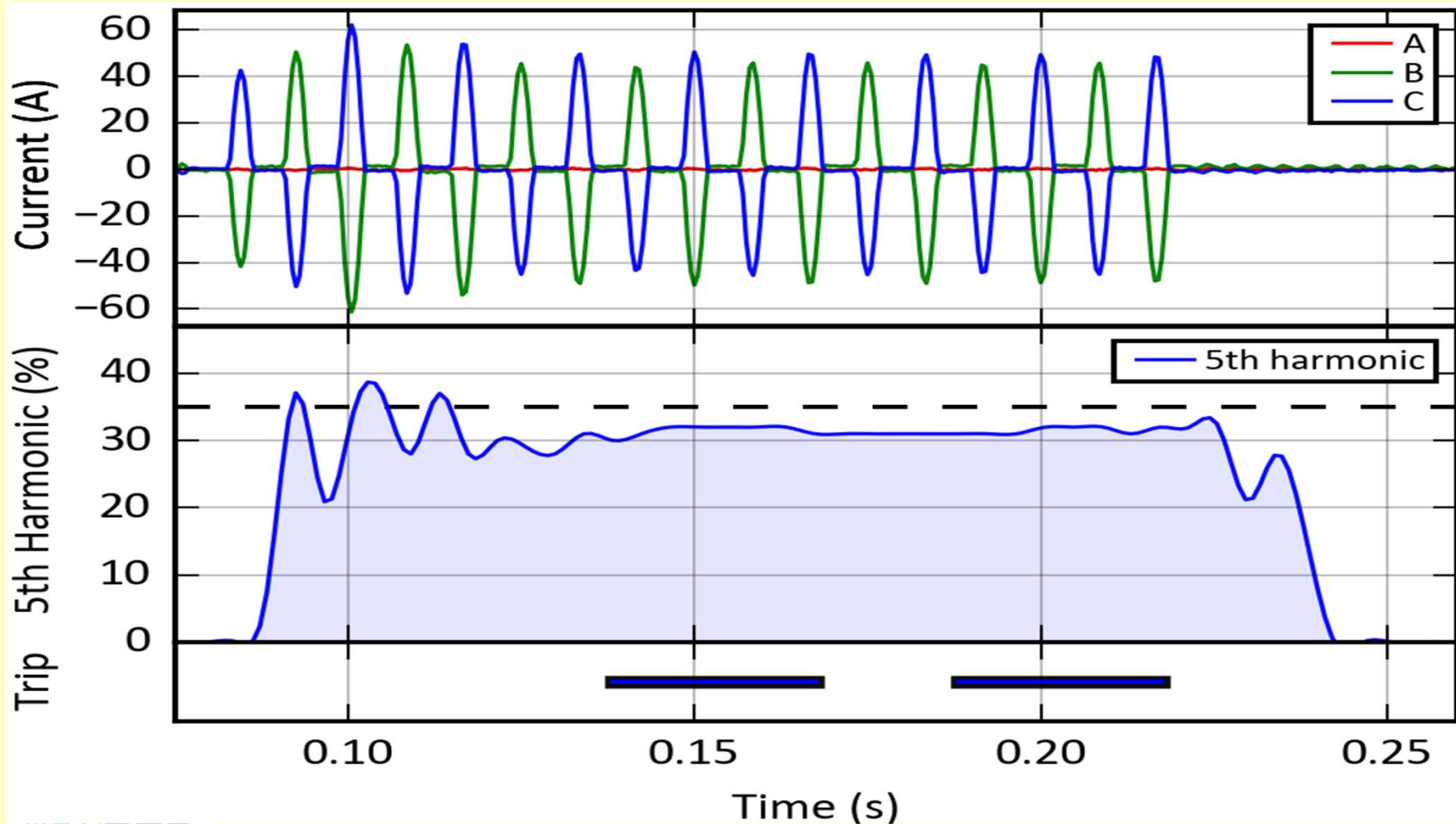
# 5<sup>th</sup> Harmonic Blocking in Differential Protection



## 5<sup>th</sup> Harmonic Blocking:

Differential relay operation is blocked when 5<sup>th</sup> harmonic distortion is more than 35%.

# BQN T3 – unfiltered event record





# BQN T3

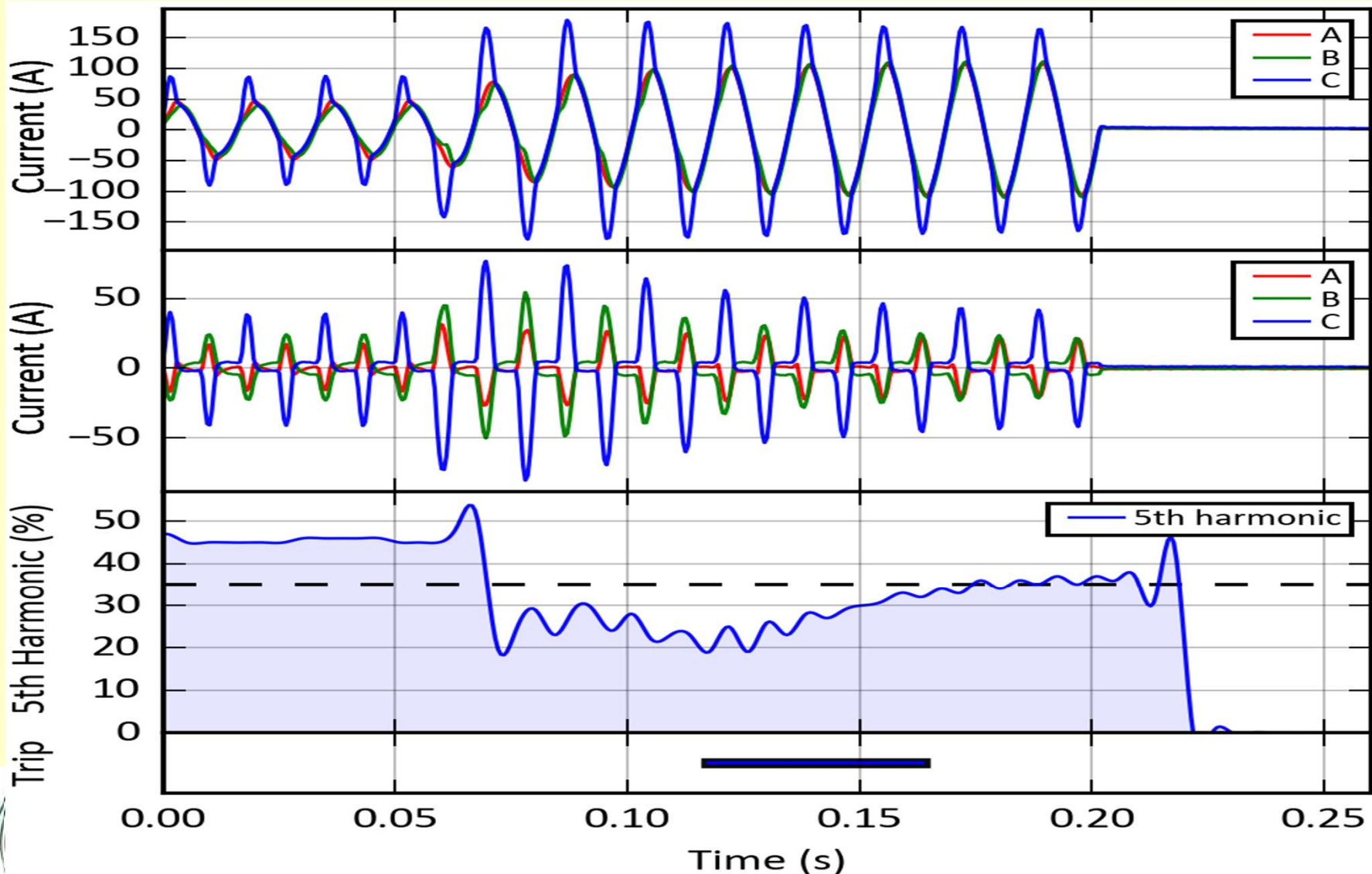
## What happened?

Over-voltage led to core saturation

- High 5<sup>th</sup> harmonic current
- Relay blocked by > 35% 5<sup>th</sup> harmonic current at onset
- Relay tripped in 3.5 cycles

Cleared BQN 2RX22 in same tripping zone

# TAT T1 – unfiltered event record



# TAT T1

## What happened?

Over-voltage led to core saturation

- High 5<sup>th</sup> harmonic current
- Relay blocked by  $> 35\%$  5<sup>th</sup> harmonic current at onset
- Relay tripped in 12.5 cycles

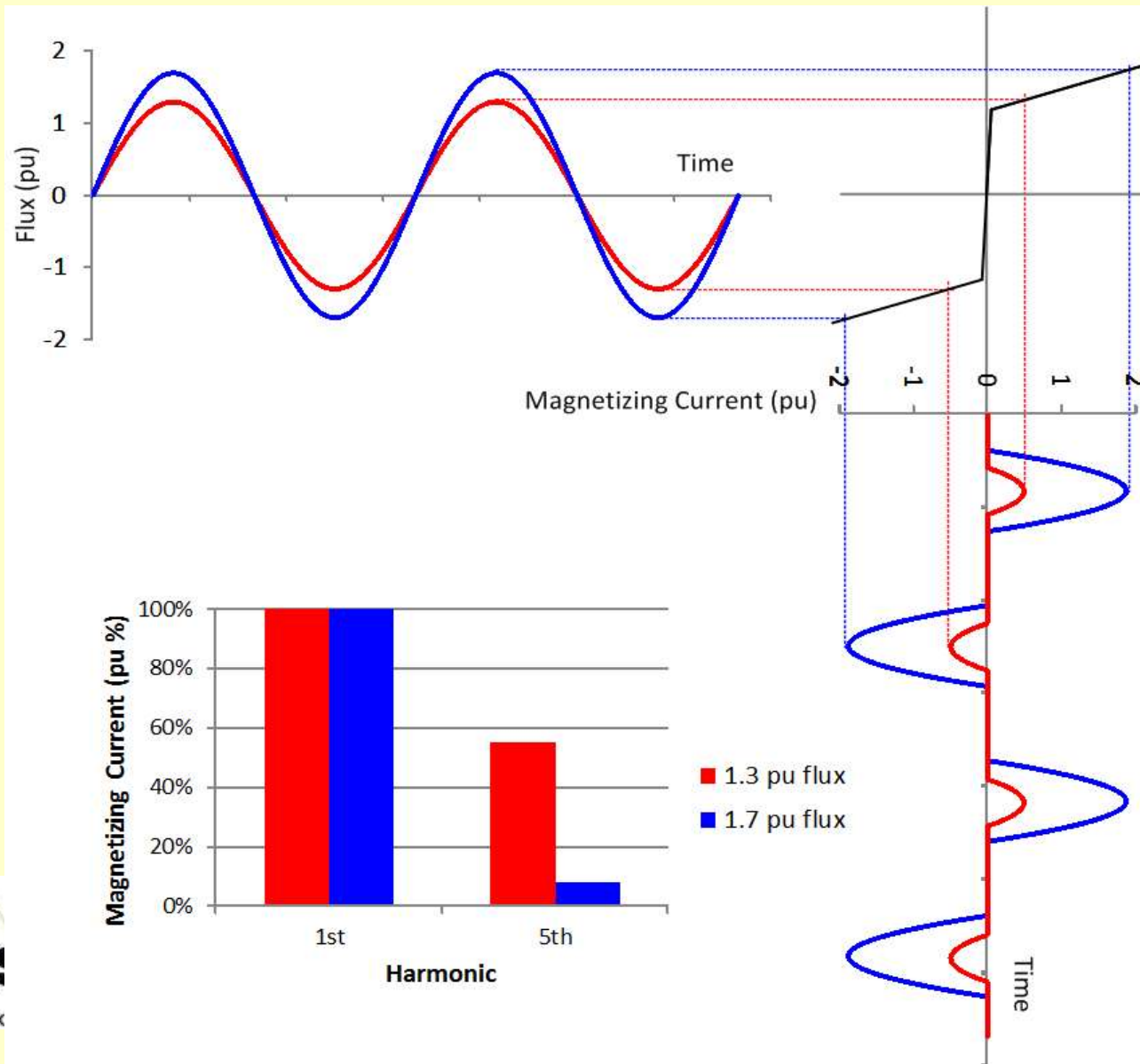
# TAT T1

## What happened?

Delta tertiary winding allowed for zero sequence current flow

System voltage began to drop as soon as TAT T1 breaker opened

# Saturation Versus Harmonic Distortion



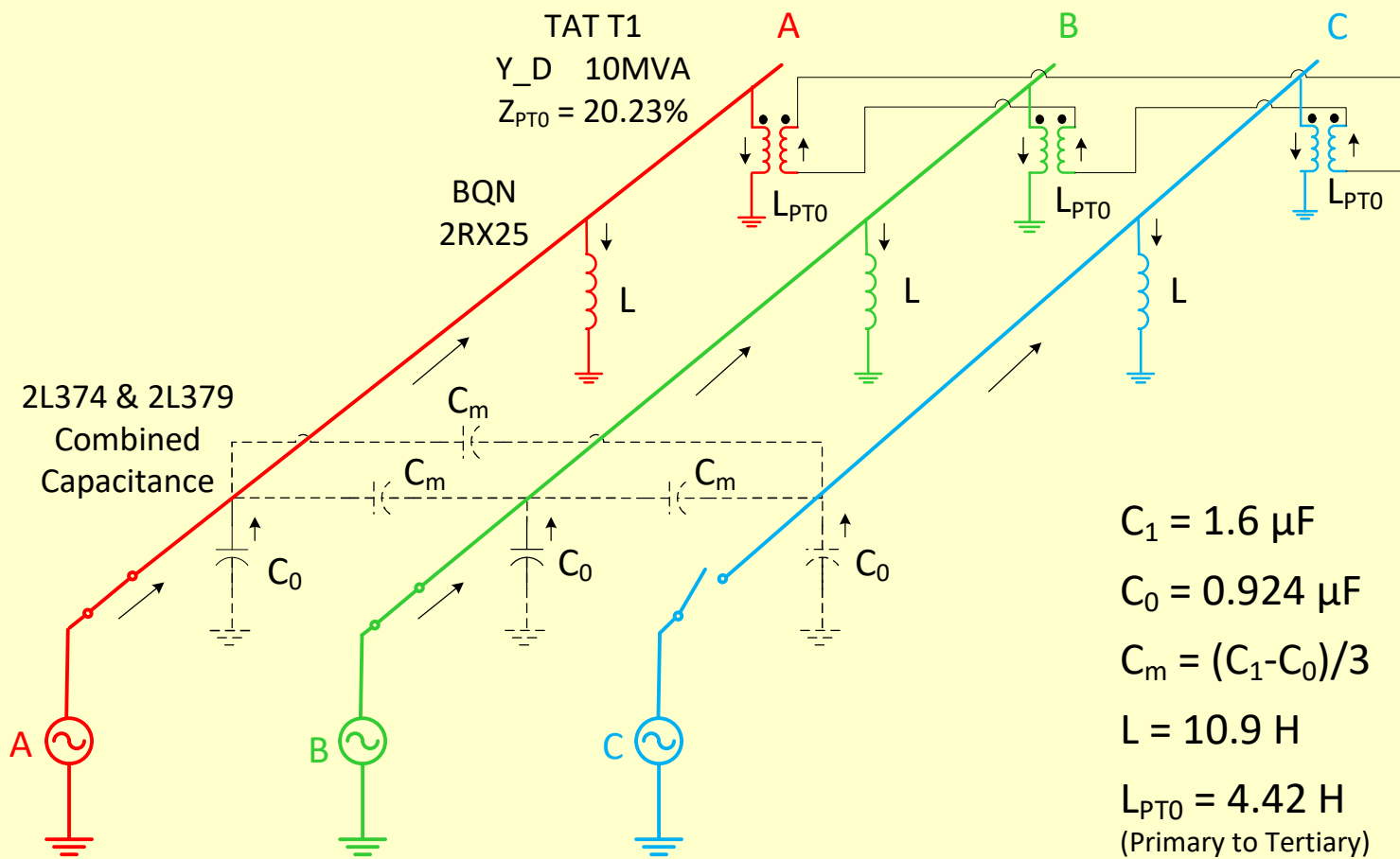
# Transformer Protection Operations

Simple graphical analysis demonstrates that the transformer differential relay with 5<sup>th</sup> harmonic blocking poses no reliability risk. With 35% blocking threshold, it can be relied on to prevent tripping for temporary overvoltages (such as 1.3 pu) yet allow tripping to “help” protect the transformer from extreme overvoltages (such as 1.7 pu) causing overexcitation.

# Analysis

Steady state, linear, and non-linear analysis

# Steady state analysis

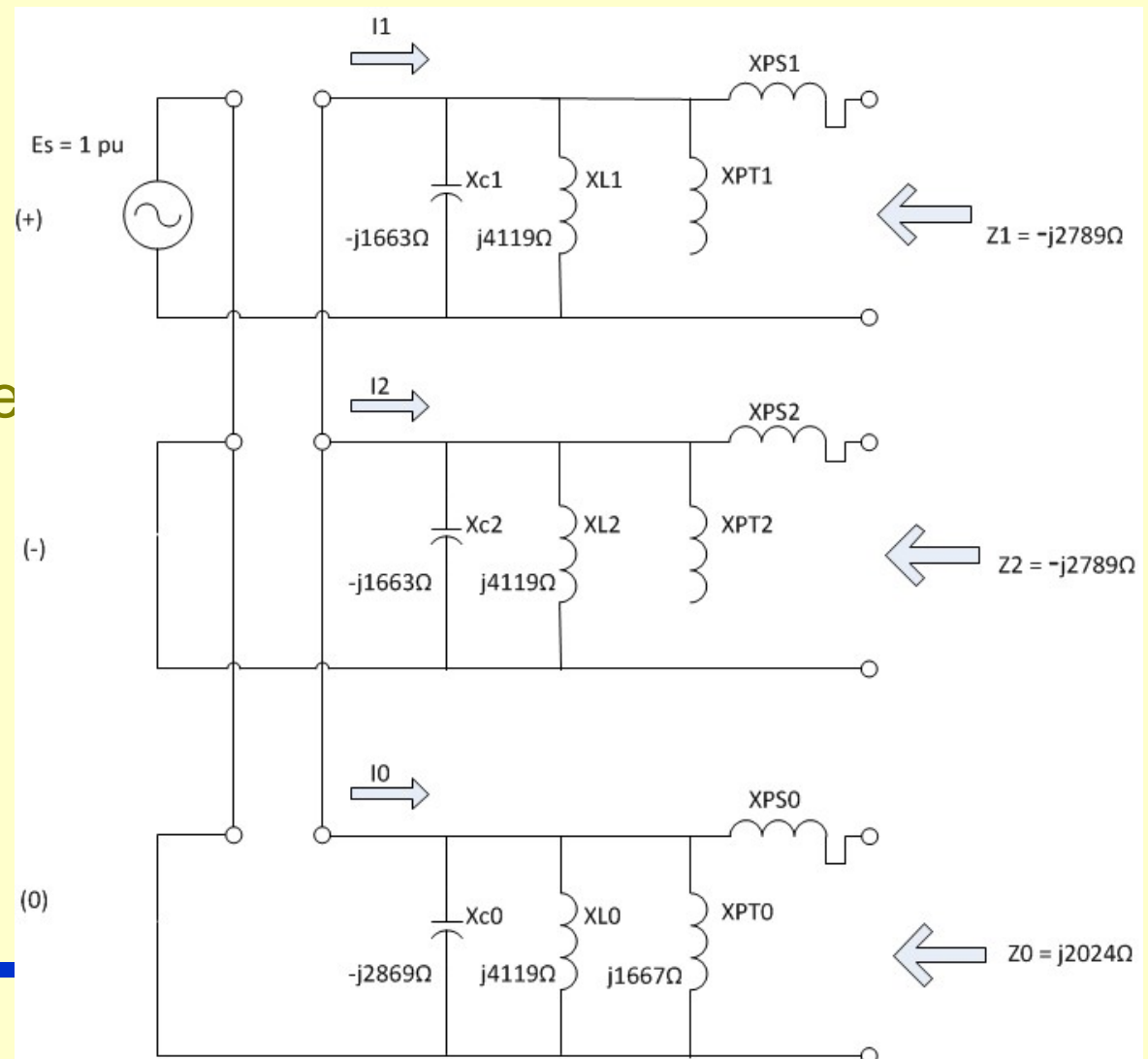


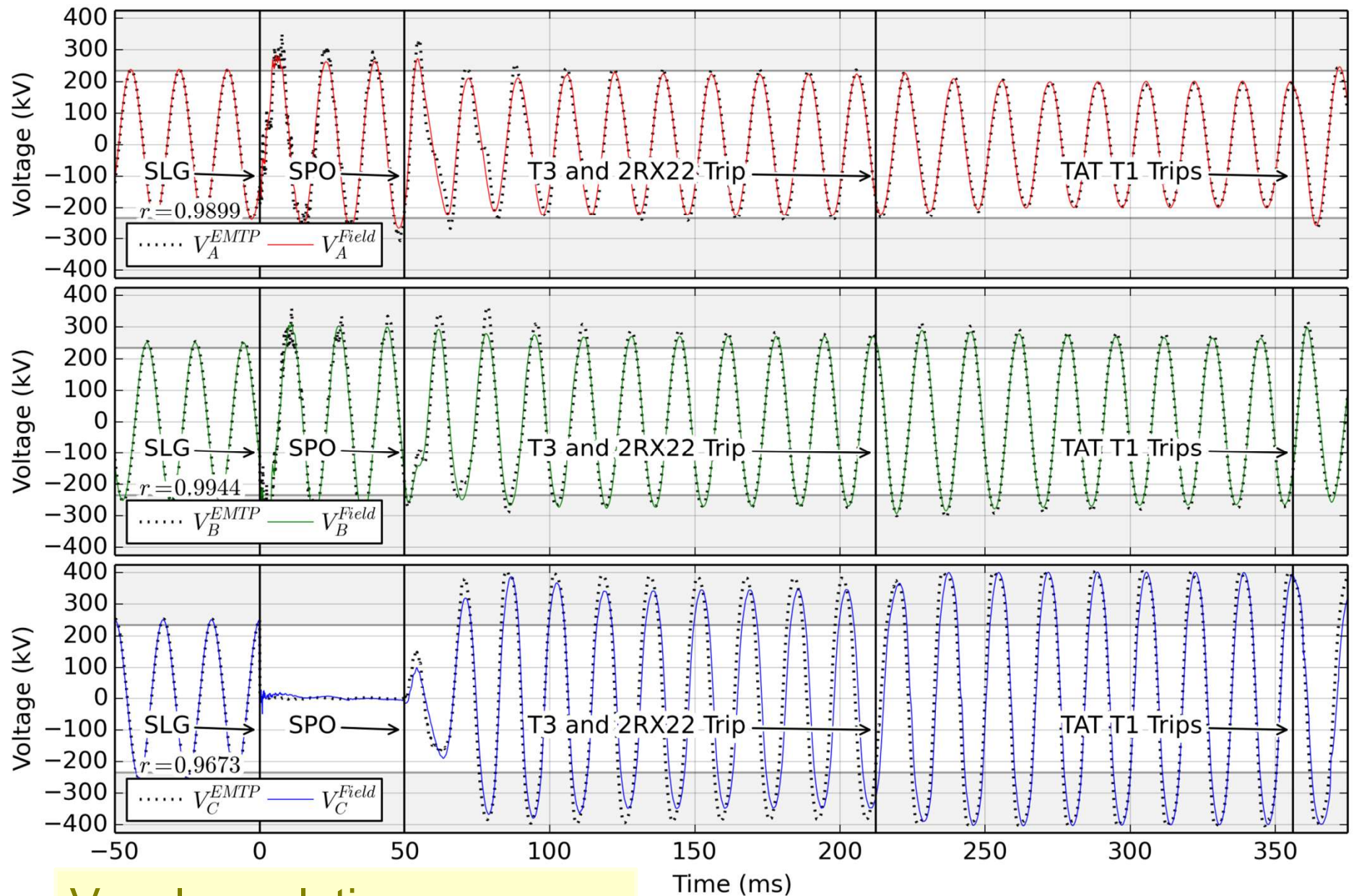


# Steady state analysis

55 Hz resonant frequency

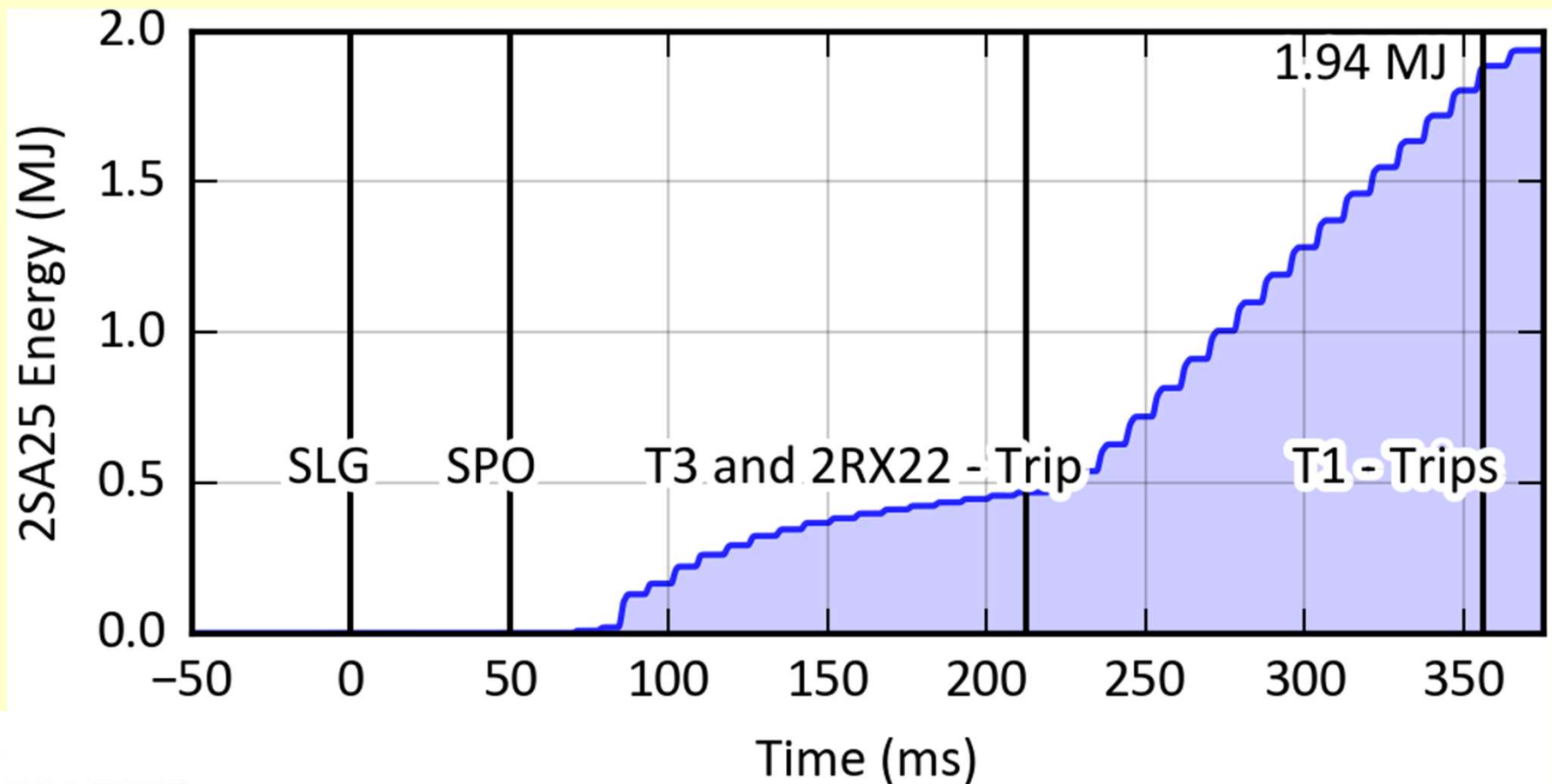
$$E_{open} = \frac{Z_1 - Z_0}{Z_1 + Z_0} E_s$$





Very low relative mean square error

# Surge Energy Absorption

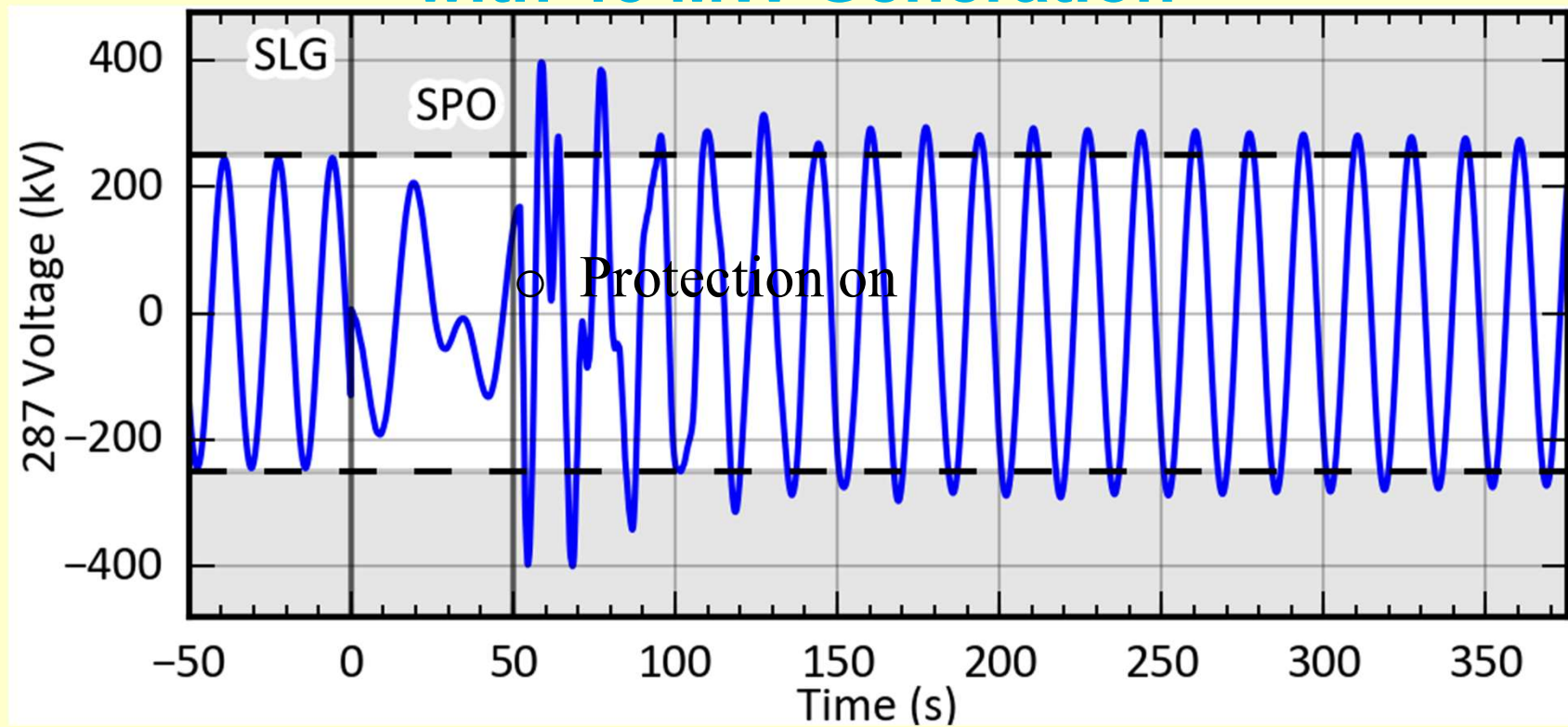


# Mitigation

Let's not do this again

# Long term solution

## EMTP simulation of single-phase open voltage with 45 MW Generation



**Single-phase trip on 2L102 is automatically disabled during periods of low generation.**

# Conclusions

Be careful applying radial single-pole tripping lines – back-energization of floating phase

The 5<sup>th</sup> harmonic blocking functions performs better than anticipated i.e. blocking is released during extreme (unsafe) overvoltages

Reinforces the benefits of performing disturbance analysis – uncover the unexpected