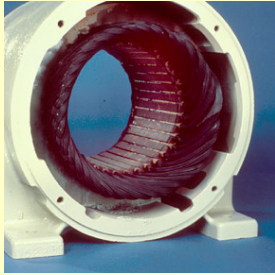


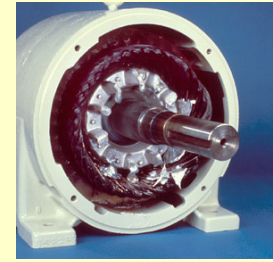
# **C37.96-2012 – IEEE guide for the Protection of AC Motor Protection**

*PSRC J10 working group, 2007-2012*

PSRC general meeting  
September, 2013

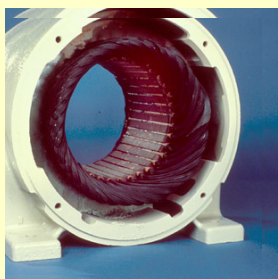


**Prem Kumar, *Chair***  
**Dale Finney, *Vice Chair***

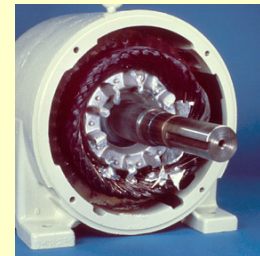


**Hasnain Ashrafi**  
**Matt Basler**  
**Steve Conrad**  
**Tom Farr**  
**Dale Frederickson**  
**Jon Gardell**  
**Wayne Hartman**  
**Nicholos Hoch**  
**Pat Kerrigan**

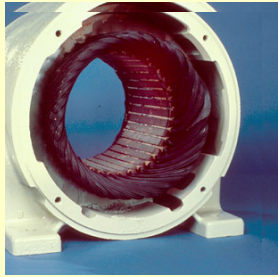
**Mohammed Khalek**  
**Jeff Long**  
**Subhash Patel**  
**Suhag Patel**  
**Mike Reichard**  
**Chris Ruckman**  
**Sam Sambasivan**  
**Sudhir Thakhur**  
**Joe Uchiyama**



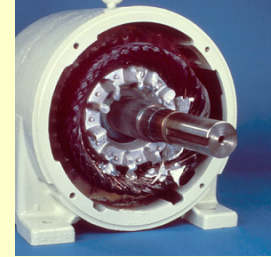
## Document Developed under PSRC



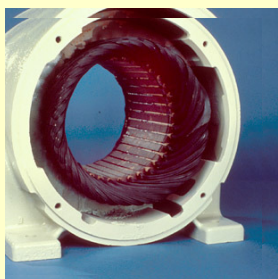
- C37.96-2012 : IEEE guide for AC Motor Protection.
- Revised and approved for publication on 5th December 2012.
- Previous revision was released in 2000



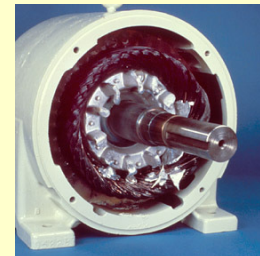
# Balloting



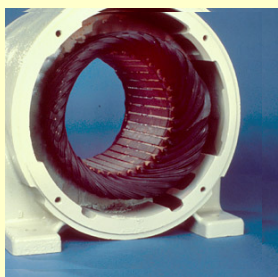
- Total 95 Balloters
- 27 Comments received, 1 negative comment
- Recirculation had 3 comments.



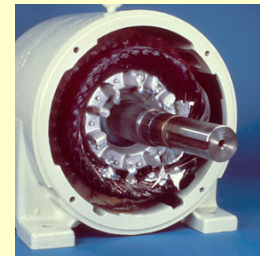
## C37.96 New items



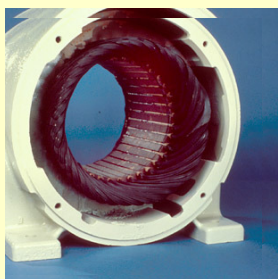
- 15 specific additions/enhancements
- ASD protection enhancements based on J1 group work
- Motor Bus transfer relevant protection issues based on J9 group work.
- Motor surge protection relevant issues
- Microprocessor relay setting example



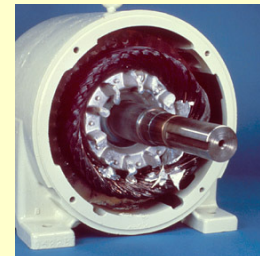
## C37.96 New items



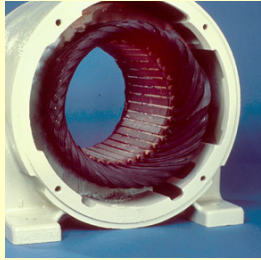
1. ASD Protection enhancements
2. Motor failure data-reasons for protection
3. Insulation class data -setting relevance
4. Motor NEMA standard data
5. Application of low ratio CTs for small motors
6. Reduced Voltage starting-setting issues
7. Motor Surge Protection
8. CT location for PF correction CAPS



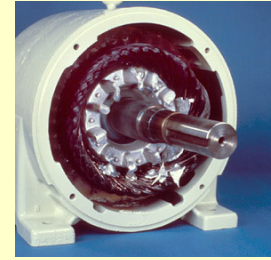
## C37.96 New items



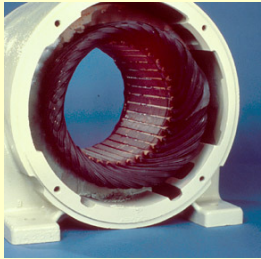
- 9. Motor Bus transfer
- 10. Motor relay/fuse coordination issues
- 11. Toroidal Ground Sensor issues
- 12. Breaker Failure Protection small motors
- 13. Understanding motor data sheets
- 14. Enhanced Motor tutorial material
- 15. Motor setting example



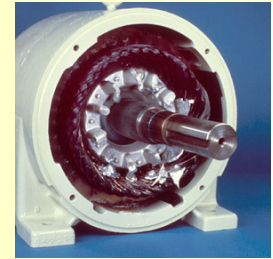
# 1a-ASD Protection Enhancements



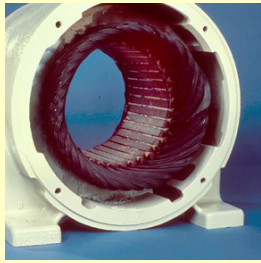
- ASD usage has increased
- ASD Controlled motors, the operating frequency impacts the motor characteristics
  - a) Starting,
  - b) Running,
  - c) Abnormal operation and fault conditions
- ASD vendors provide motor protection functions part of drive system



# 1b-ASD System Issues

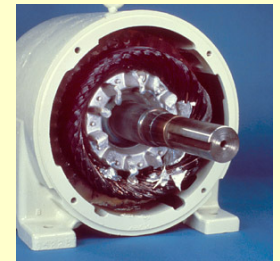


- Better process control-ability to vary process speed
- Efficiency-affinity laws power savings
- Soft Start Capability
- Short Circuit Current Reduction
- Bus transfer issues
- Issues with PF correcting CAPS



# 1c- ASD and Motor System

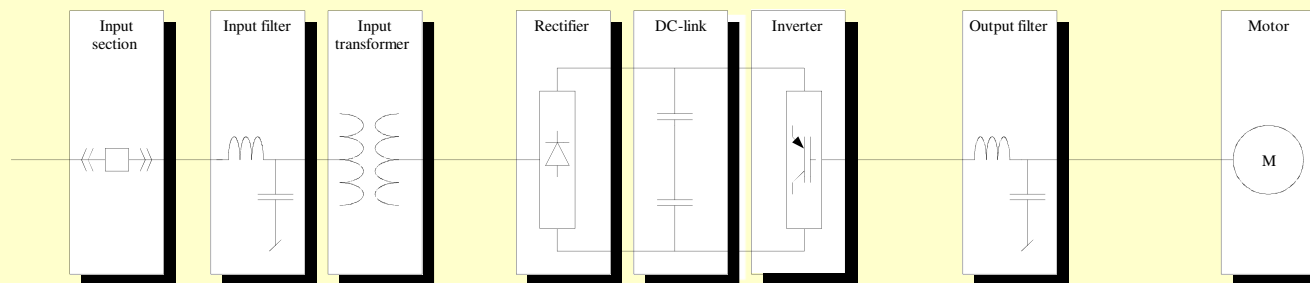
## Basic Blocks of an ASD

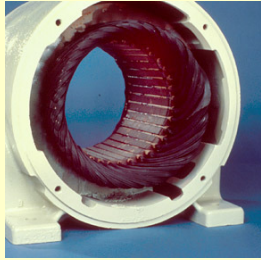


Input: Zone 1  
Transformer

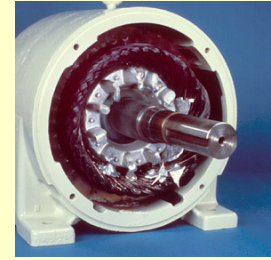
Drive: Zone 2  
Power Electronics

Output: Zone 3  
Motor





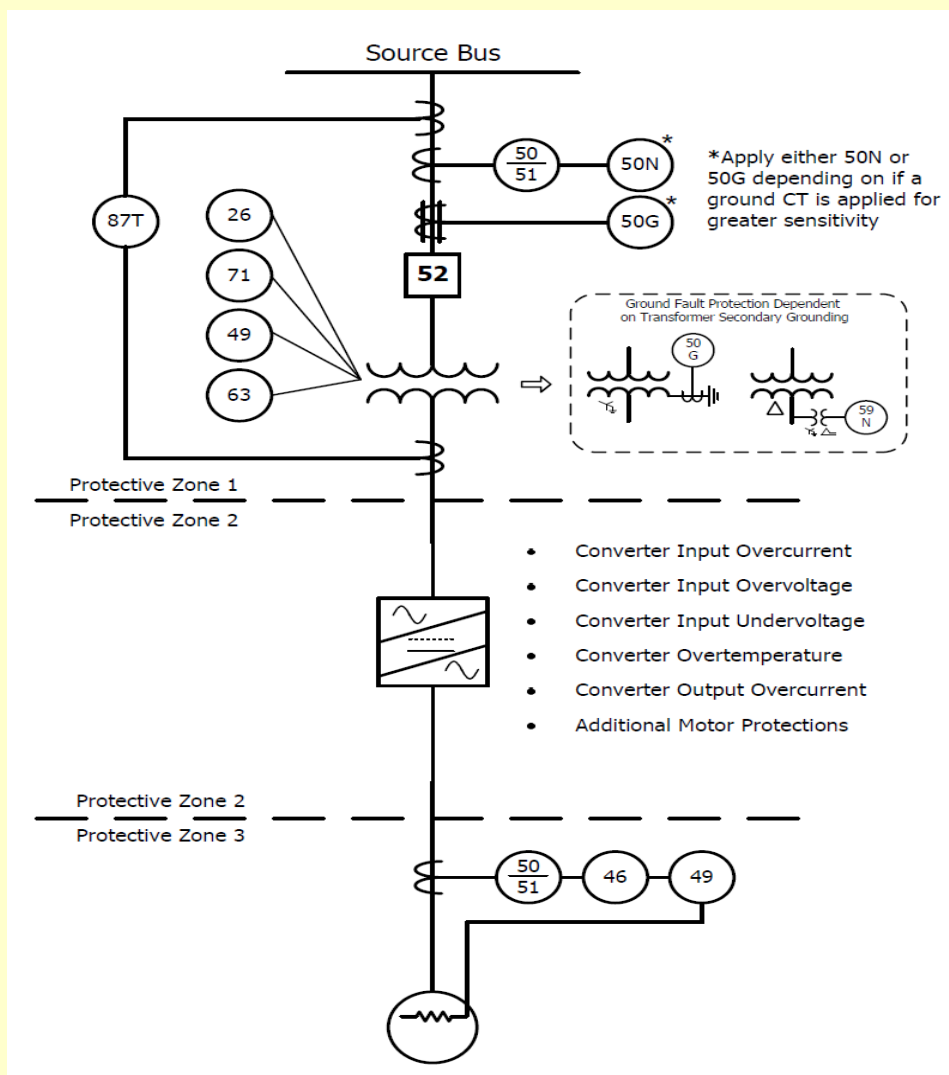
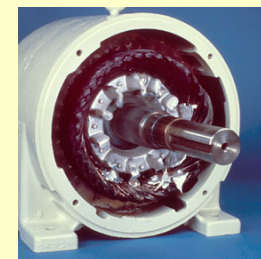
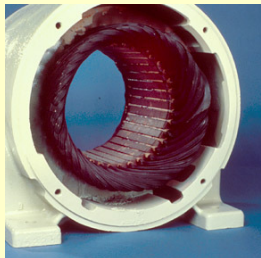
# 1d-ASD Protection Enhancements

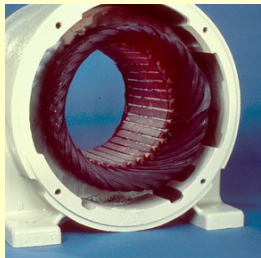


## Adjustable-Speed Motor Protection

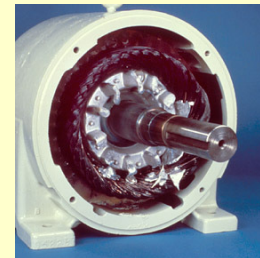
- Three zone Protection strategy
  - Zone 1 Input Transformer Protection
  - Zone 2 Power Electronics Protection
  - Zone 3 Motor Protection

# 1e- ASD Protection zones



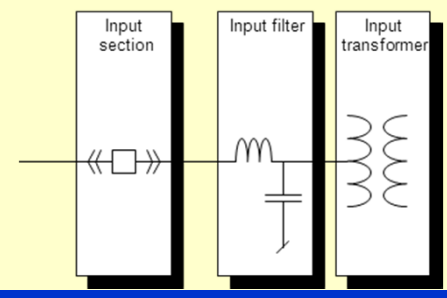


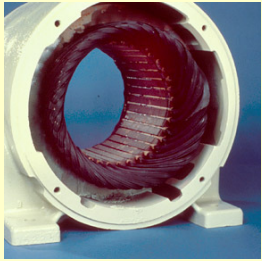
# 1 f-ASD Protection Zone 1



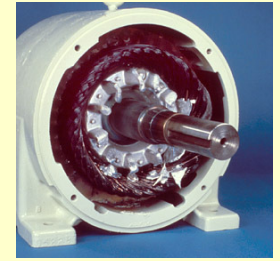
## Adjustable-Speed Motor Protection

- Overcurrent protection
- Limitations of differential protection for multi winding transformers
- Issues with Zone 1 protections are harmonics, co-ordination with supply breaker, for multi winding transformer differential protection



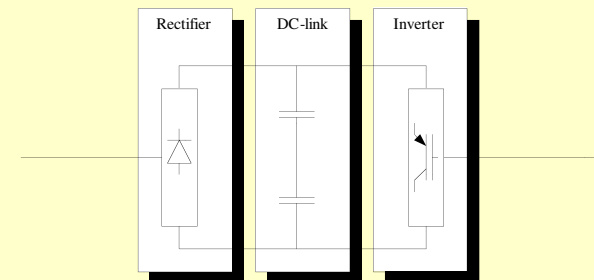


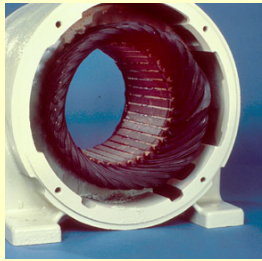
## ASD Protection Zone 2 Issues



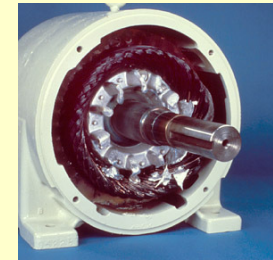
The ASD vendor provides this area of protection for power electronics including rectifier, DC link and inverter

- DC Bus over voltage
- DC Bus under voltage
- Rectifier and Inverter over temperature
- Loss of control power
- Converter over current
- Inverter over current
- Additional Motor Protections

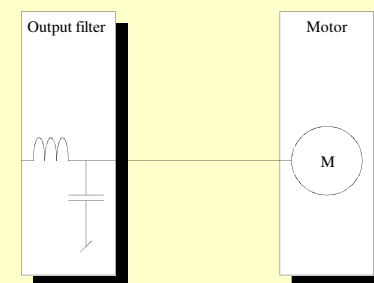


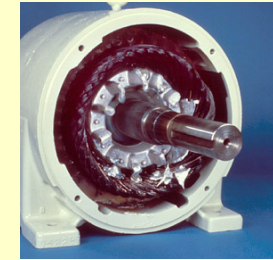
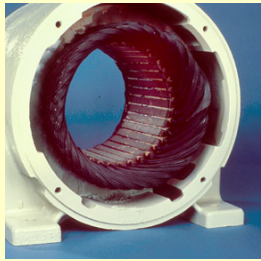


## ASD Protection Zone 3 issues



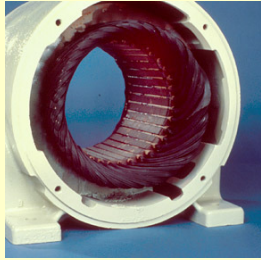
- Thermal model of motor has limited value
- CTs saturate at low frequency
- Frequency capability of relay is important consideration depends on where process operates
- For large motors consider additional protection
  - Overcurrent.
  - Differential
  - Ground protection





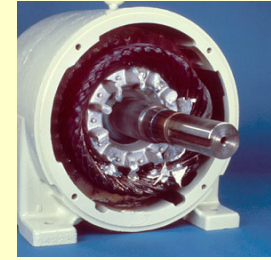
## 2-Motor Failures data

Failed Component	Induction Motors	Synchronous Motors	Wound Rotor Motors	Direct Current Motors	Total (All Types) Numbers	Total (All Types) Percentage	Protection
Bearings	152	2	10	2	166	43.7%	38, 39
Windings	75	16	6	-	97	25.56%	26, 46, 49, 50, 50N, 51, 51N, 51R, 59, 87
Rotor	8	1	4	-	13	3.4%	21, 26, 46, 49, 50, 50N, 51, 51N, 51R, 59, 87
Shaft or Coupling	19	-	-	-	19	5.0%	37, 39
Brushes or Slip Ring	-	6	8	2	16	4.2%	40, 53, 55
External Devices	10	7	1	-	18	4.7%	27, 32, 40, 47, 53, 55, 60, 63, 64, 78, 81
Not Specified	40	9	-	2	51	13.4%	
Total	304	41	29	6	380	100%	N/A



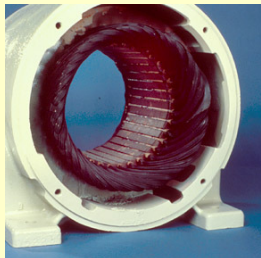
## 3a-Insulation Class (NEMA)

Service factor = 1



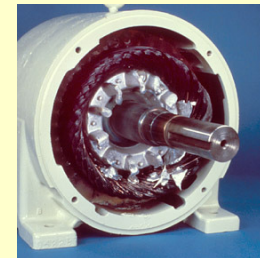
Machine Rating	Temperature Measurement	Insulation Class °C			
		A	B	F	H
All horsepower ratings	RTD	60	80	105	125
≤ 1500 hp	Embedded Detector*	70	90	115	140
> 1500 hp and ≤ 7 kV		65	85	110	135
> 1500 hp and > 7 kV		60	80	105	125

\*Embedded detectors are located within the slot of the machine and can be either resistance elements or thermocouples

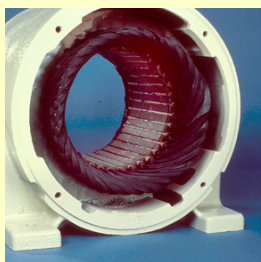


## 3b-Insulation Class (NEMA)

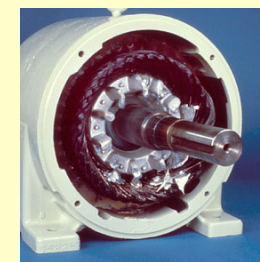
Service factor = 1.15



Machine Rating	Temperature Measurement	Insulation Class °C			
		A	B	F	H
All horsepower ratings	RTD	70	90	115	135
≤ 1500 hp	Embedded Detector*	80	100	125	150
> 1500 hp and ≤ 7 kV		75	95	120	145
> 1500 hp and > 7 kV		70	90	115	135

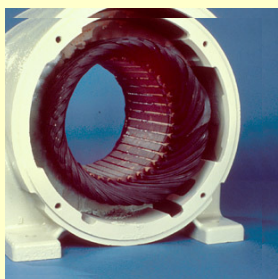


## 4-Motor Characteristics (NEMA)

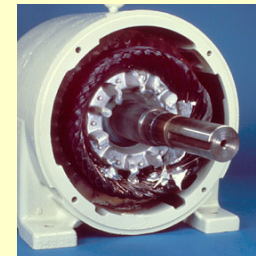


Design	Locked Rotor Torque *	Pull-up Torque*	Breakdown Torque*	LR Current*	Slip %
A	70-275	65-190	175-300	Not defined	0.5-5
B	70-275	65-190	175-300	600-800	0.5-5
C	200-285	140-195	190-225	600-800	1-5
D	275	Not defined	275	600-800	≥5
IEC H	200-285	140-195	190-225	800-1000	1-5
IEC N	75-190	60-140	160-200	800-1000	0.5-3

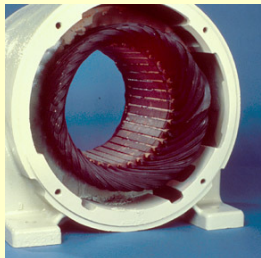
\* percent of rated load torque or load current



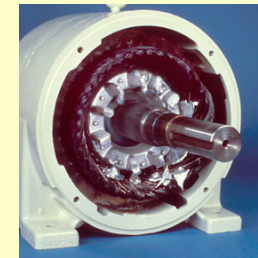
## 5-Application of low ratio CTs



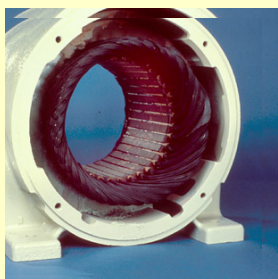
- MV buses with high fault currents and small motors need careful attention for CT sizing.
- CT sizing evaluated for proper protection operation.
- Could require a separate high ratio CT be used for SC protection.
- MV contactors with fuses low ratio CT Ok.
- Modern microprocessor relay advanced algorithms can provide correct phasor estimation during high current faults.



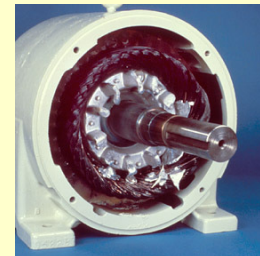
## 6-Reduced Voltage Starting



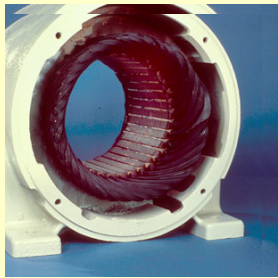
Starter Type	% Motor Voltage During Start	% Motor Current at Locked Rotor	% Line Current at Locked Rotor	% Torque at Locked Rotor
<b>Primary Reactor</b>				
80% Tap	80	80	80	64
65% Tap	65	65	65	42
50% Tap	50	50	50	25
<b>Auto Transformer</b>				
80% Tap	80	80	64	64
65% Tap	65	65	42	42
50% Tap	50	50	25	25
<b>Wye/Delta Start</b>				
Wye Start	58	58	33	33



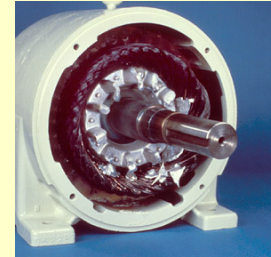
## 7a-Surge Protection



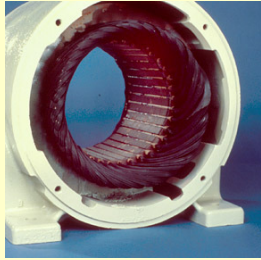
- Types of insulation-Ground wall and turn
- Steady state and steep fronted voltages
- Motor Surge Capability Withstand Requirements from NEMA MG-1-2009 and IEC 60034-15-15: 2009
- Equivalent NEMA and IEC BILs for commonly used Motor Voltages
- Various Surge Protection Techniques and Features



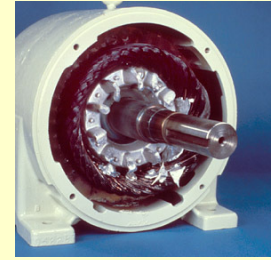
## 7b-Surge Protection Techniques



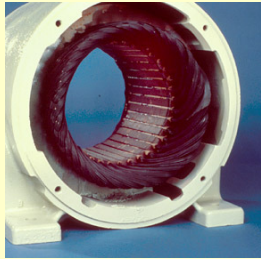
- Effective shielding of overhead lines supplying the plant.
- Surge Arrestors at the motor terminals.
- Surge Capacitors at the motor terminals.
- Low ground resistance at the service entrance and supply switchgear.
- Single end grounding at the motor or supply end depending on cable shielding / raceway / arrangement.



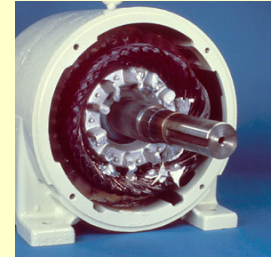
## 8 PF CAP CT Location



- CT placed before the PFCC
  - CT will see motor amps minus PFCC amps
  - Less accurate for OL setting
  - Protection can clear PFCC faults
- CT placed after the PFCC
  - CT will see motor amps
  - Upstream protections need to detect PFCC faults

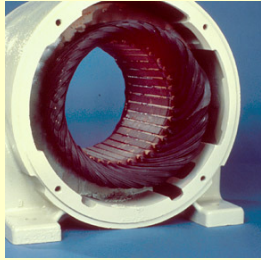


## 9a-Motor Bus Transfer (MBT)

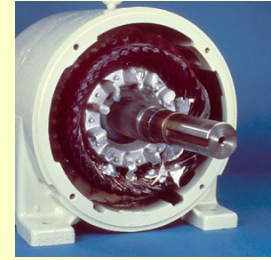


Required to maintain continuity of critical processes in a generating or industrial plant during the following periods

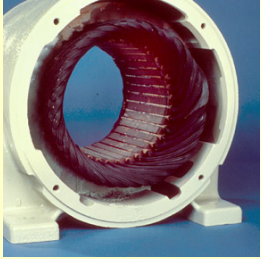
- Planned transfers
  - Maintenance or startup/shutdown
- Emergency transfers
  - Loss of present source due to a fault



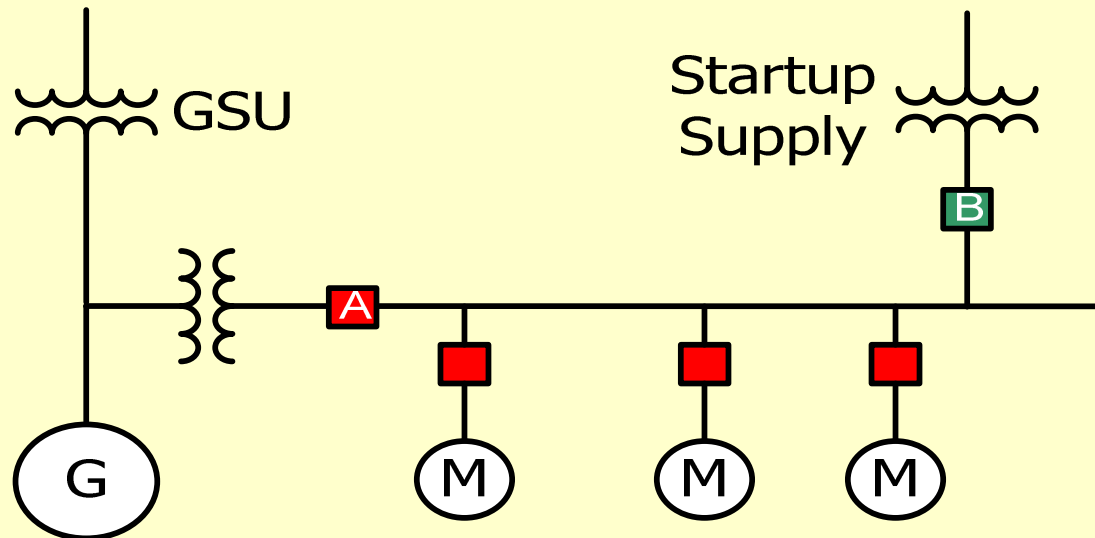
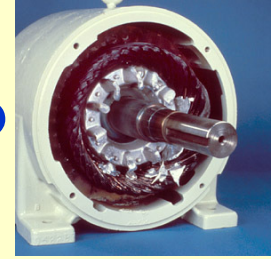
## 9b-Risk to Motors



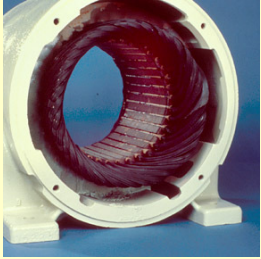
- A poor transfer can result in a significant angle between the new source and the motor bus at the instant of closing.
  - This results in very high transient torque and current.
  - Damage can be immediate or cumulative.



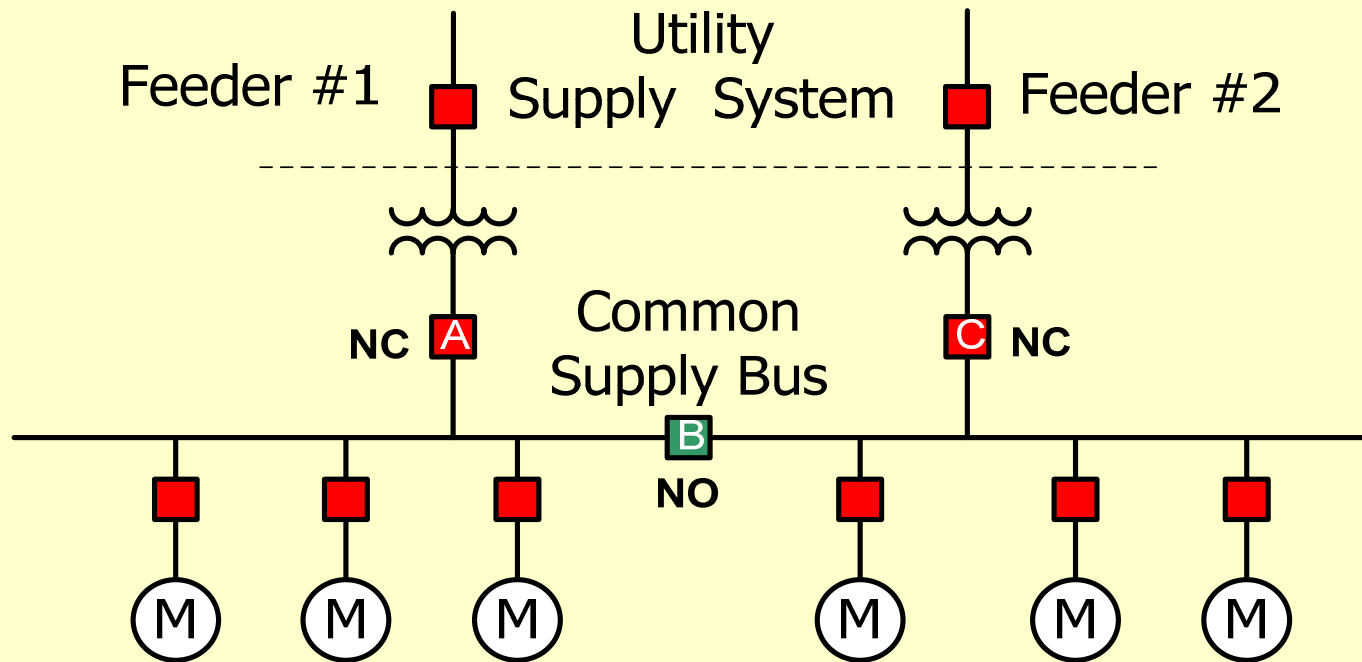
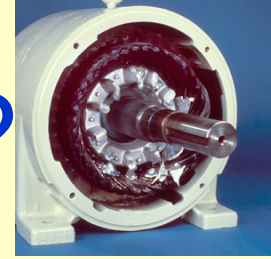
## 9c-Where is MBT needed?



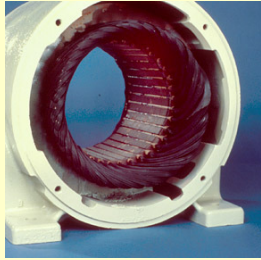
### Unit Connected Generator



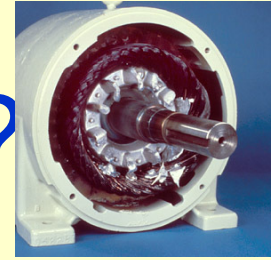
## 9d-Where is MBT needed?



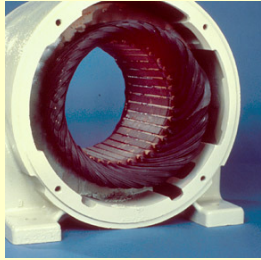
# Industrial Facilities



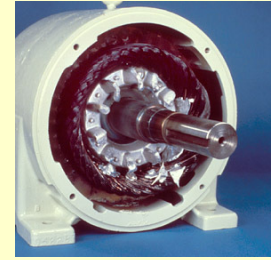
## 9e-When it is needed?



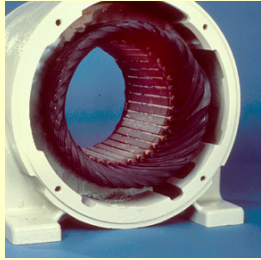
- Planned transfers
  - Maintenance or startup/shutdown
- Emergency transfers
  - Loss of existing source due to a fault



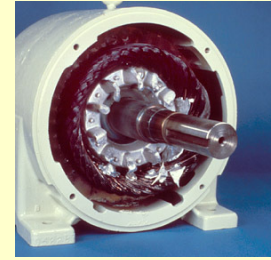
# 9f-Types of MBT



- **Closed Transition**
  - Hot Parallel Transfer
- **Open Transition**
  - Fast
  - In-Phase
  - Residual Voltage

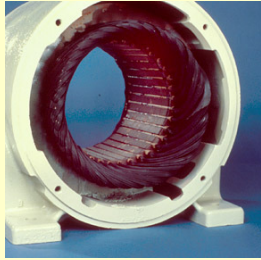


# 9g-Hot Parallel Transfer

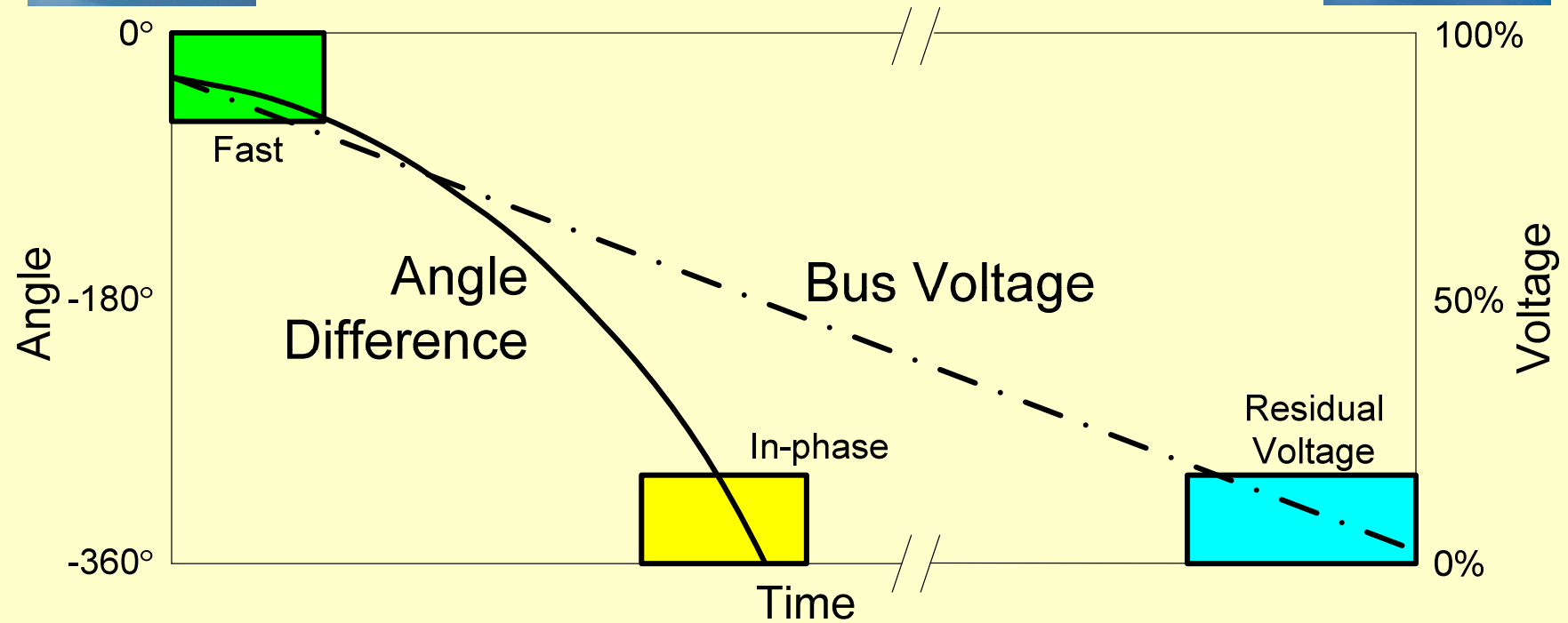
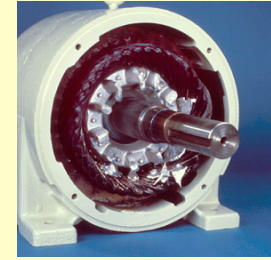


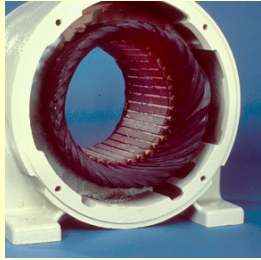
## Steps:

1. Check synchronism
  2. Check that new source voltage is acceptable
  3. Close new source breaker
  4. Open old source breaker
- Ensure that paralleling is temporary
  - Cannot be used for emergency transfer

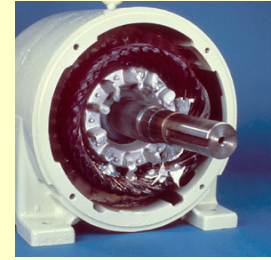


# 9h-Open Transfers

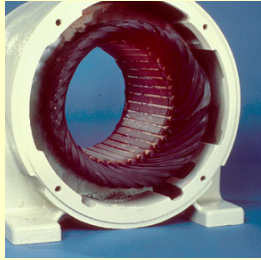




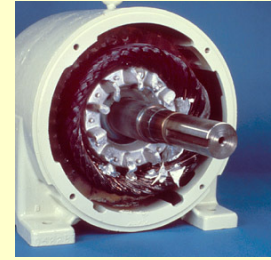
# 9i-Fast Transfer



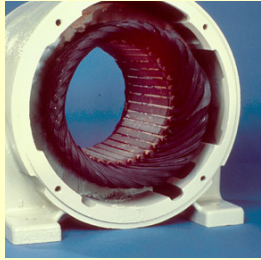
- Requires sync-check supervision and possibly a high-speed sync-check
- Checks upper/lower voltage on the new source
- Must continuously check for rapidly changing conditions across the open new source breaker



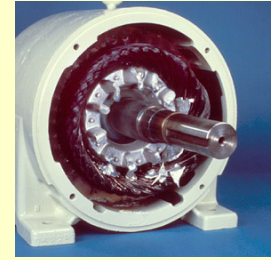
# 9j-In-Phase Transfer



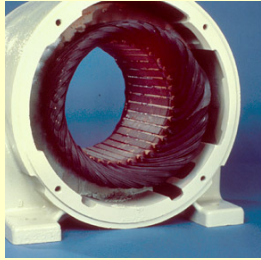
- Predicts movement toward synchronism between the motor bus and the new source
- Checks upper/lower voltage on the new source and slip frequency
- Must compensate for breaker closing time



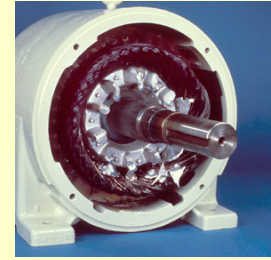
# 9k-Residual Transfer



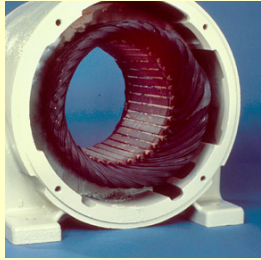
- Unsupervised as to phase angle or slip frequency,
- Checks that bus voltage is below lower limit ( $\sim < 0.25$  pu).
- Frequency may decay past the motor stall point - load shedding may be required



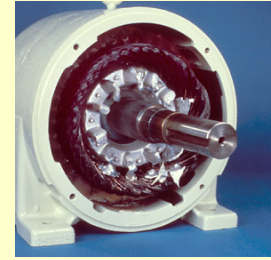
## 10a-Application of Fuses



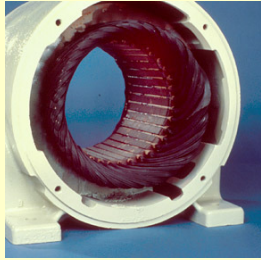
- Medium voltage, Class E2 starters, IEEE C37.46 – 2010, R-Rated current limiting fuses provides short circuit protection.
- Preferred standard interruption rating is 40 or 50 kA symmetrical per UL 347 – 2009.



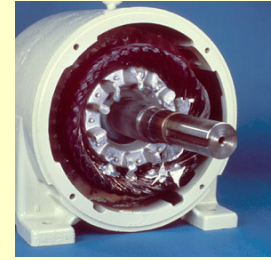
## 10b-Application of Fuses



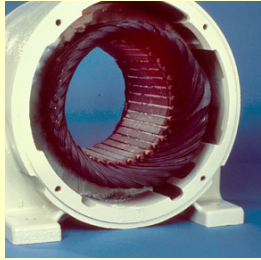
- Fuse fatigue is a major concern for starting of large motors.
  - Select a fuse whose melting time is 125% of the acceleration time of the motor with its load connected at the locked rotor current value.
  - If unknown assume LRA to be six times FL and acceleration=10 sec.



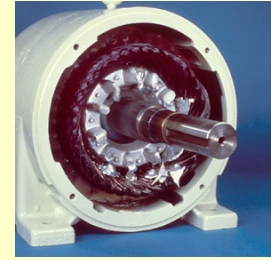
## 10c-Application of Fuses



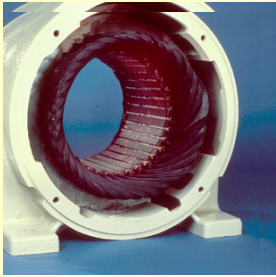
- For fused contactor applications
  - Size CTs for OL conditions only
  - OL relay protection is not intended operate to interrupt fault.
- Therefore CT saturation is not of great concern
  - CL fuse is sized to interrupt fault



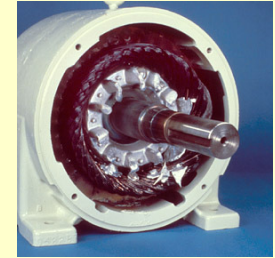
## 11-Ground Sensor Relay



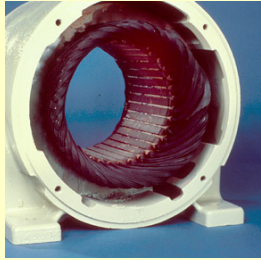
- Supplied by a core-balance CT to provide sensitive protection (5-12 A)
- Limited by the capacitive unbalance
- Asymmetrical breaker pole closing combined with the cable/motor/surge capacitance produces current transient.
- lightning or switching surge can also cause a trip.



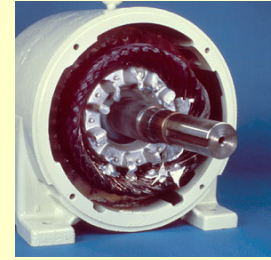
## 12. Breaker Failure Protection



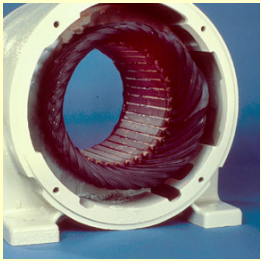
- Needed because backup relay pickup (switchgear incomers) could still be less than locked rotor current and cannot sense motor feeder breaker failure.
- Can occur for small motors



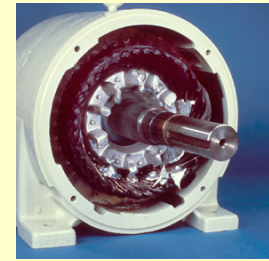
## 13a-Deriving settings from Nameplate and Data Sheets



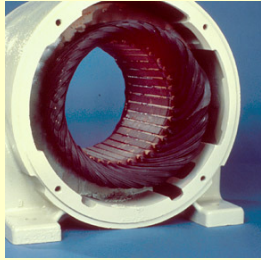
- These parameters provide the information necessary to configure various thermal and short circuit protection elements
- For medium/large motors thermal damage curves are typically provided and starting curves at rated and reduced voltage



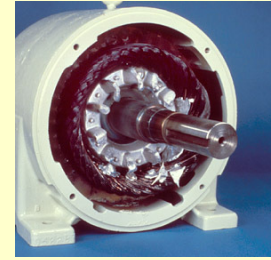
## 13b-Available Data



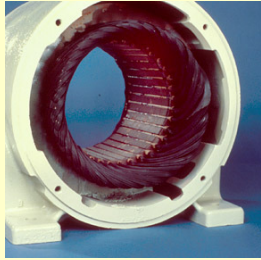
- Full load current
- Locked rotor amps
- Safe stall time at ambient temp
- Safe stall time at operating temp
- Maximum ambient temperature and rated temperature rise or insulation class
- Cooling time constants



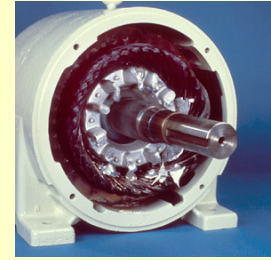
## 13c-How is it used?



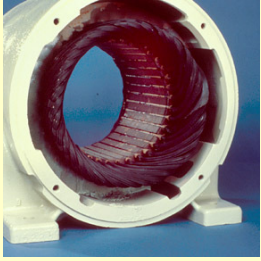
- In some cases the data is entered directly into the relay.
- In other cases procedures are provided for deriving the settings



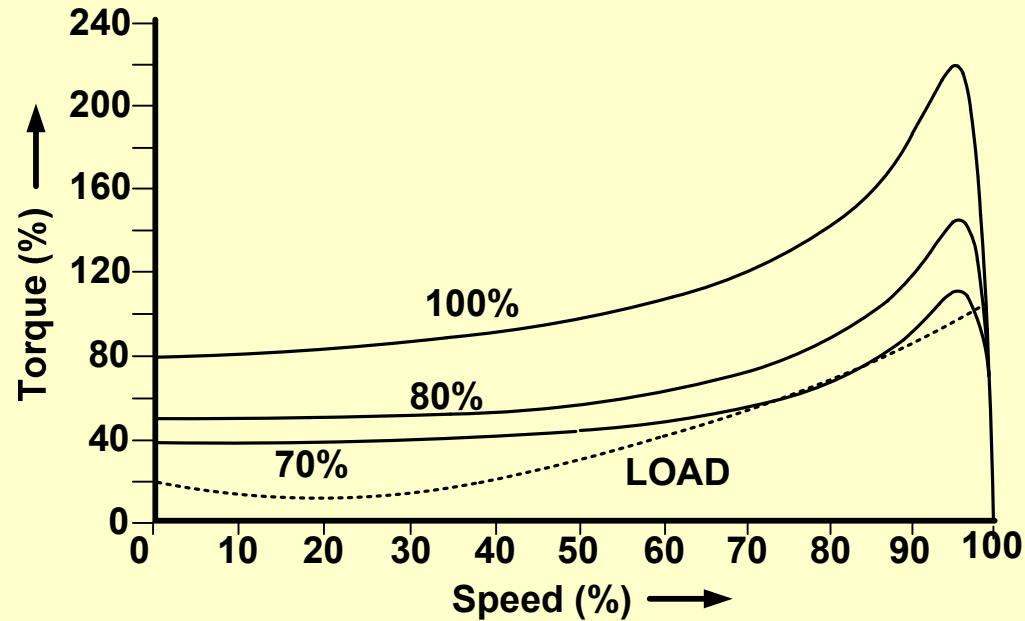
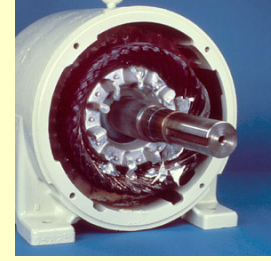
## 13d-Other Functions



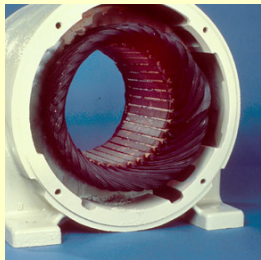
- Maximum starts per hour or minimum time between starts can be entered to protect the motor against frequent starting
- If cooling times are unavailable, the relay may be able to learn the cooling time based on the motor state and RTD measurements



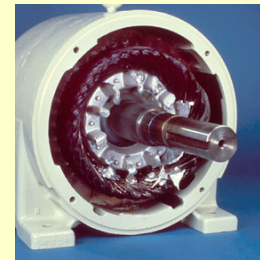
# 14-Annex Material



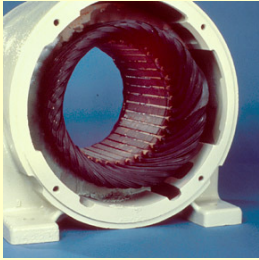
- Acceleration Time
- Voltage Dip Calculation and Resulting Torque



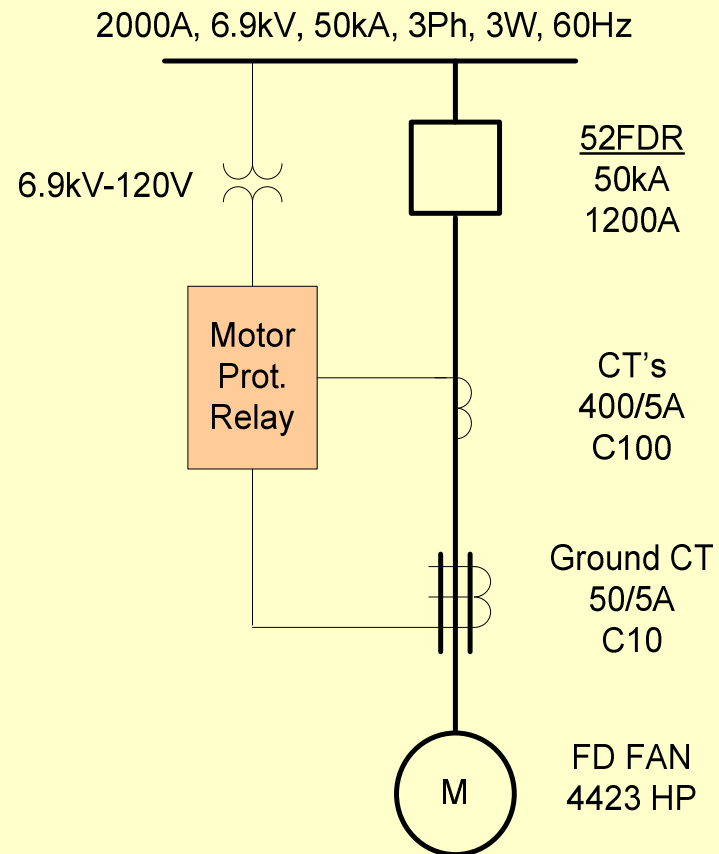
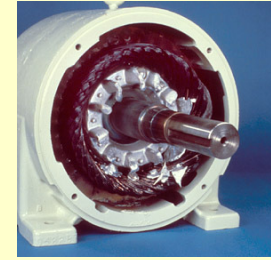
# 15a-Relay Setting Example

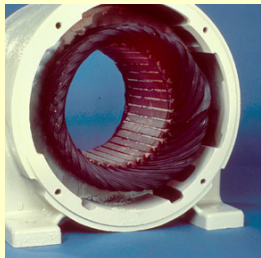


- Annex A-3 added to show how to set multifunction motor protection relay
- Source for input data for determining various settings
  - Single Line Diagram for CT, VT ratio, system information
  - Motor Data Sheet for motor information
  - Motor Thermal Curve
- calculate each setting from available data.

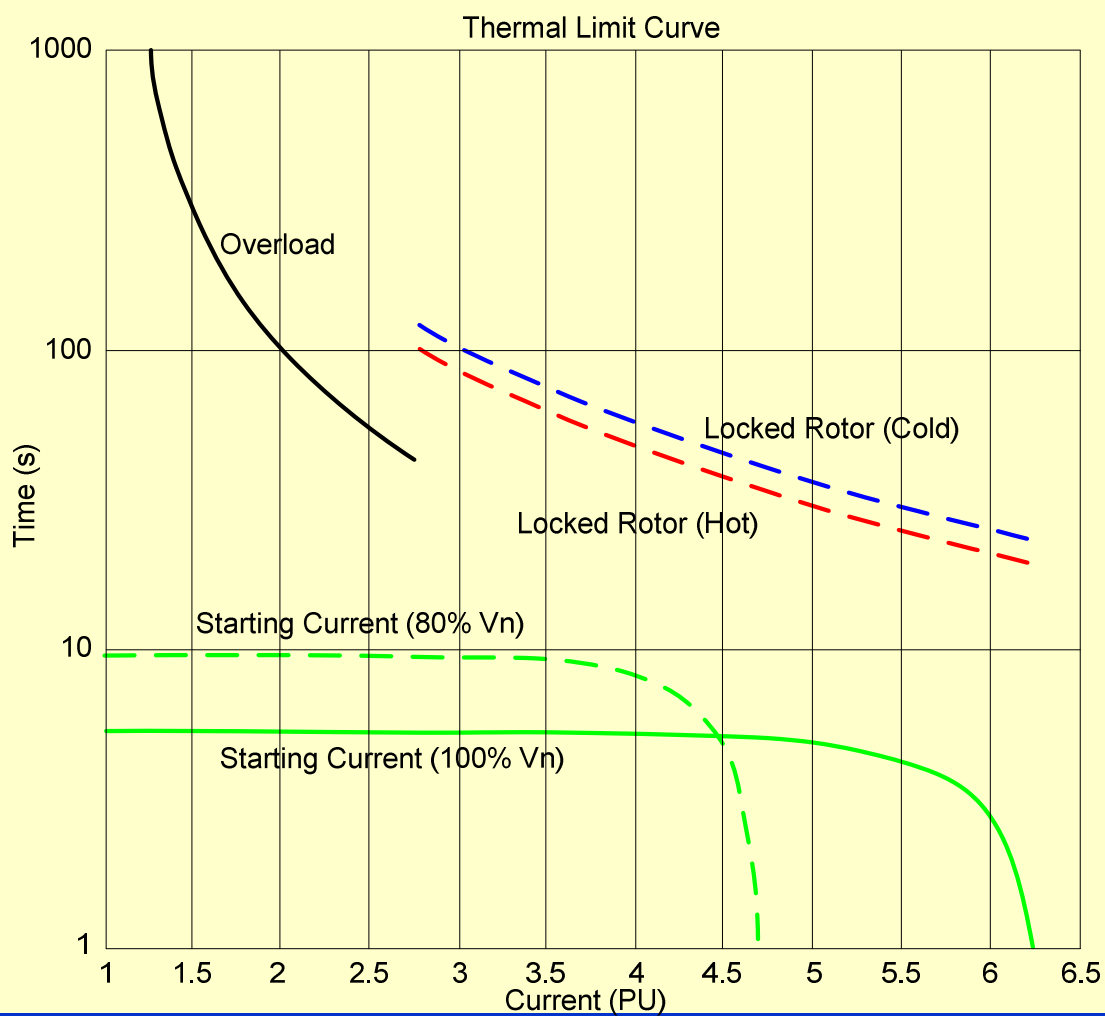
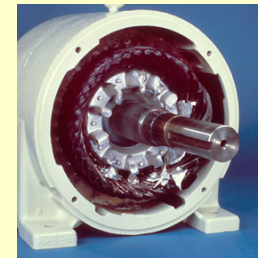


## 15b-Relay Setting Example





# 15c-Relay Setting Example



# *Thanks*

# Questions?